

MANITOBA HVDC RESEARCH CENTRE,
a Division of Manitoba Hydro International Ltd.

Renewable Device Modeling and Harmonic Model Derivation using PSCAD™/EMTDC™

October 19, 2017

Presented by: Kumara Mudunkotuwa
Mathias Pielahn

Renewable Device Modeling

- Electromagnetic transient (EMT) vs. RMS simulations
- Generic and detailed vendor models
 - Focus on: Type 3 & Type 4 wind turbines, PV inverters
 - Switching and average models
- Collector network aggregation

Harmonic Model Derivation

- Methodology of harmonic injection
- Interpretation and implication of results

EMT vs. RMS Simulations

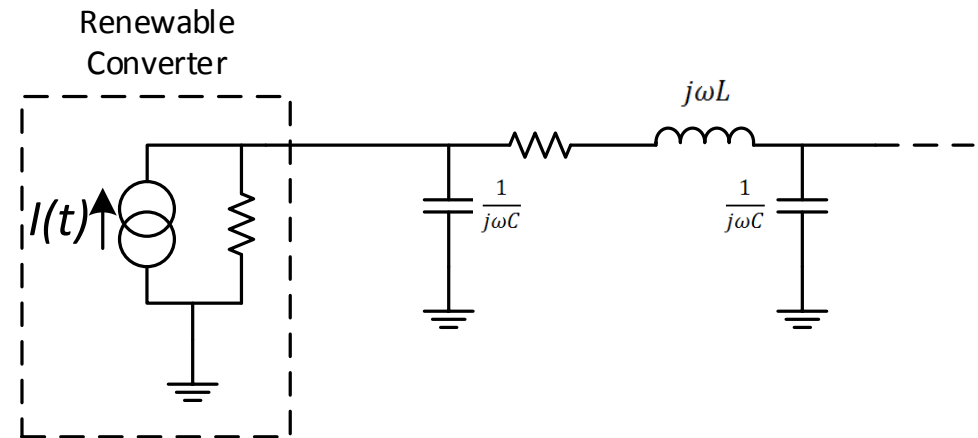
Why EMT models are important in studies involving renewables?

- RMS modeling does not represent the network dynamics.
 - Any phenomena caused by converter interaction with the network is not captured accurately.
- EMT modeling is able to capture these network dynamics accurately.
 - SSR, SSCI, fault ride through in weak grid, harmonic resonances in the collector network, etc.

EMT vs. RMS Simulations

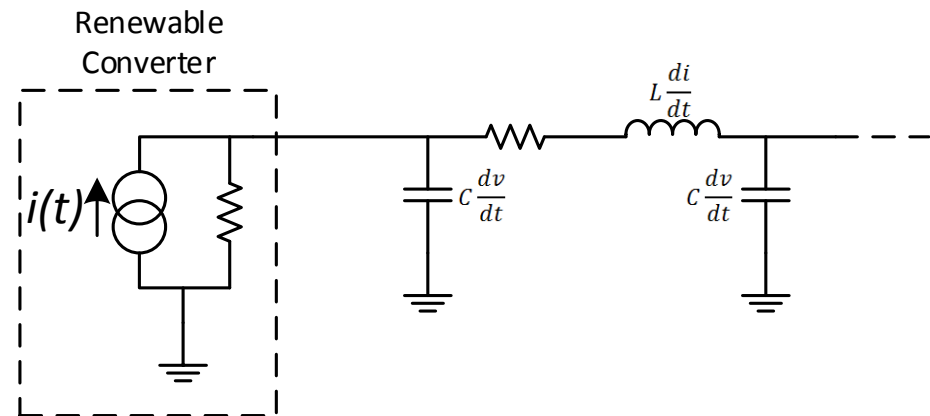
RMS

- Assume quasi-steady state
- Network transients neglected
- Fundamental phasor solution
- Positive sequence
- Large network possible



EMT

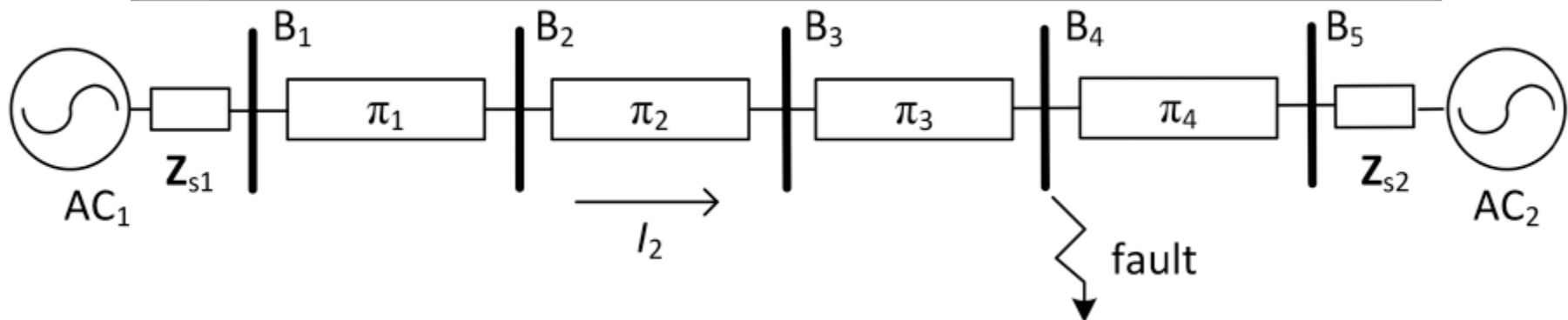
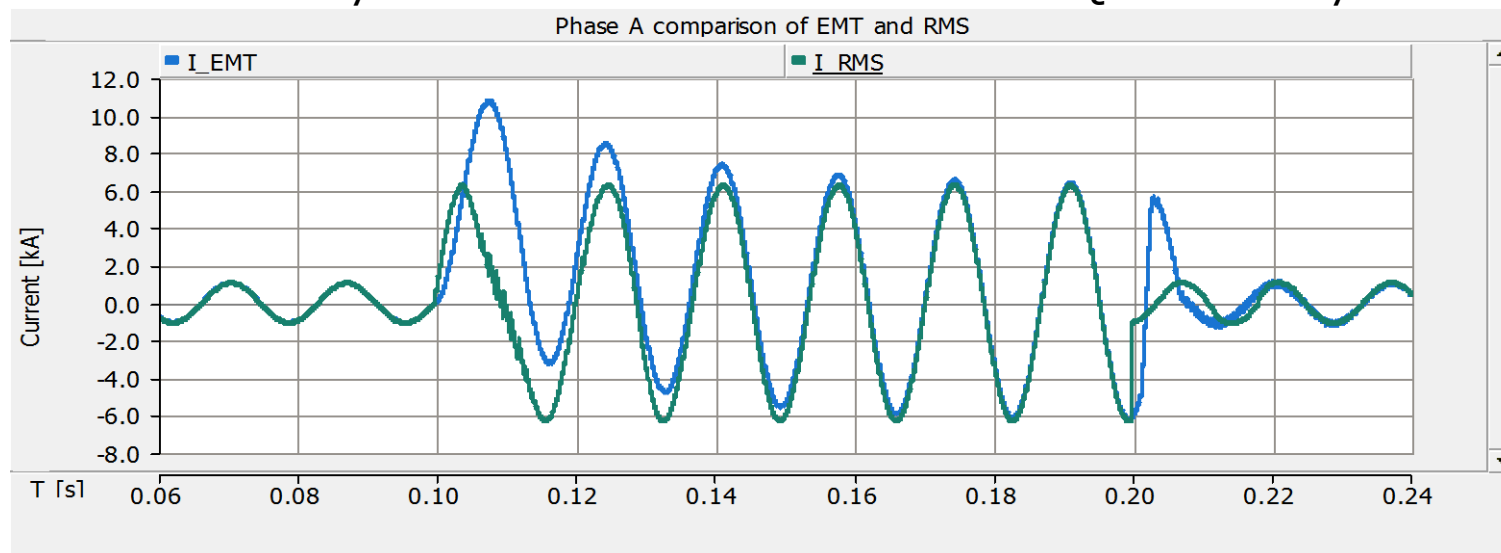
- Consider differential equations
- Numerical integration substitution
- Upper freq. depends on simulation time step (0~MHz)



EMT vs. RMS Simulations

Example:

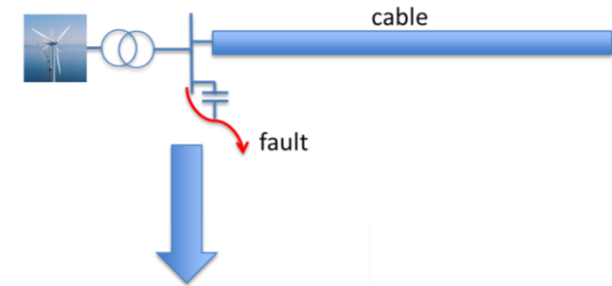
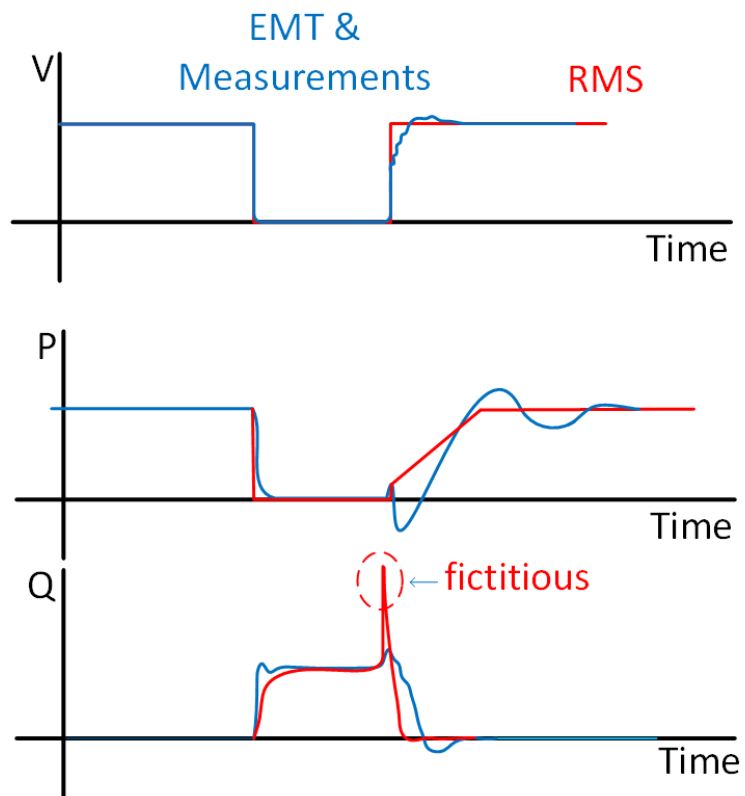
- EMT solutions may have DC offset other high frequency transients
- RMS has the steady state solution of each instant → Quasi-steady state



EMT vs. RMS Simulations

Example:

- EMT is able to capture the dynamics during a fault accurately.
- RMS results follow the fundamental.



Generic vs. Detailed Vendor Models

Generic vs. Detailed Vendor Models

Generic model

- Does not represent any particular vendor model/equipment.
- Will provide typical or generic type of response.
- Used in system planning studies (for which individual model details are not crucial), or when modeling nearby wind/PV farms that don't require particular detail.

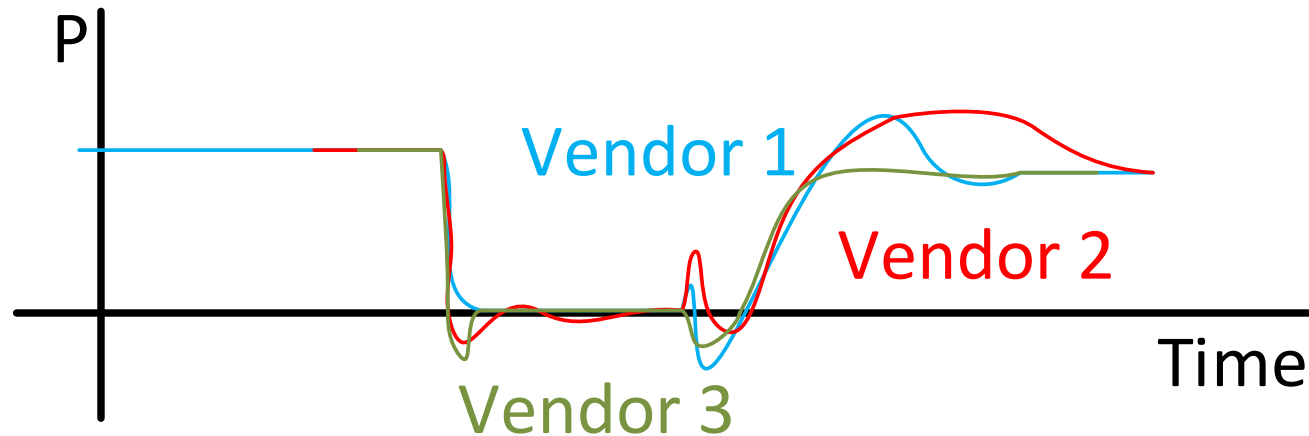
Vendor model

- Represents particular details of equipment.
- Often these details are intellectual property.
 - Thus, models are 'black-boxed' to hide sensitive algorithms.
- Used in interconnection studies and studies involving grid code compliance, SSR/SSCI, tuning controllers etc.

Generic vs. Detailed Vendor Models

Vendor model

- Different vendor models have significantly different dynamics responses.
- Pre- and post-fault steady state responses may be similar.
- Therefore, the appropriate vendor models are always recommended to be used in detailed EMT studies.

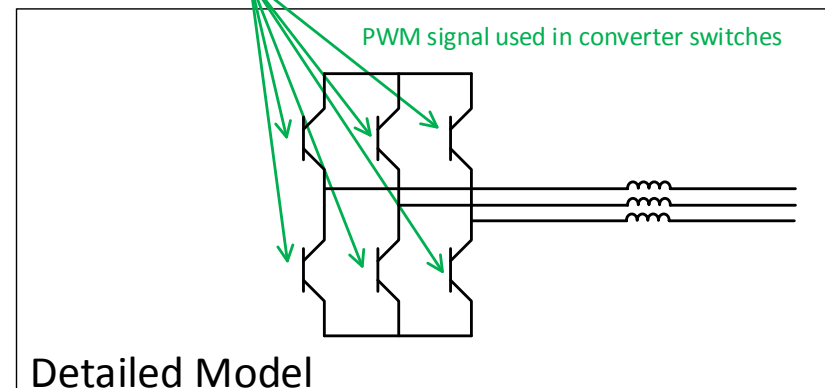
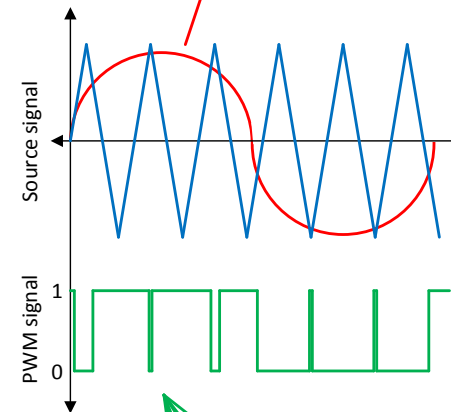
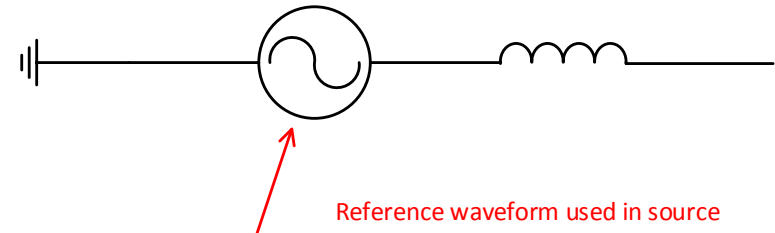


Average Model vs. Detailed Model

Average model vs. Detailed model

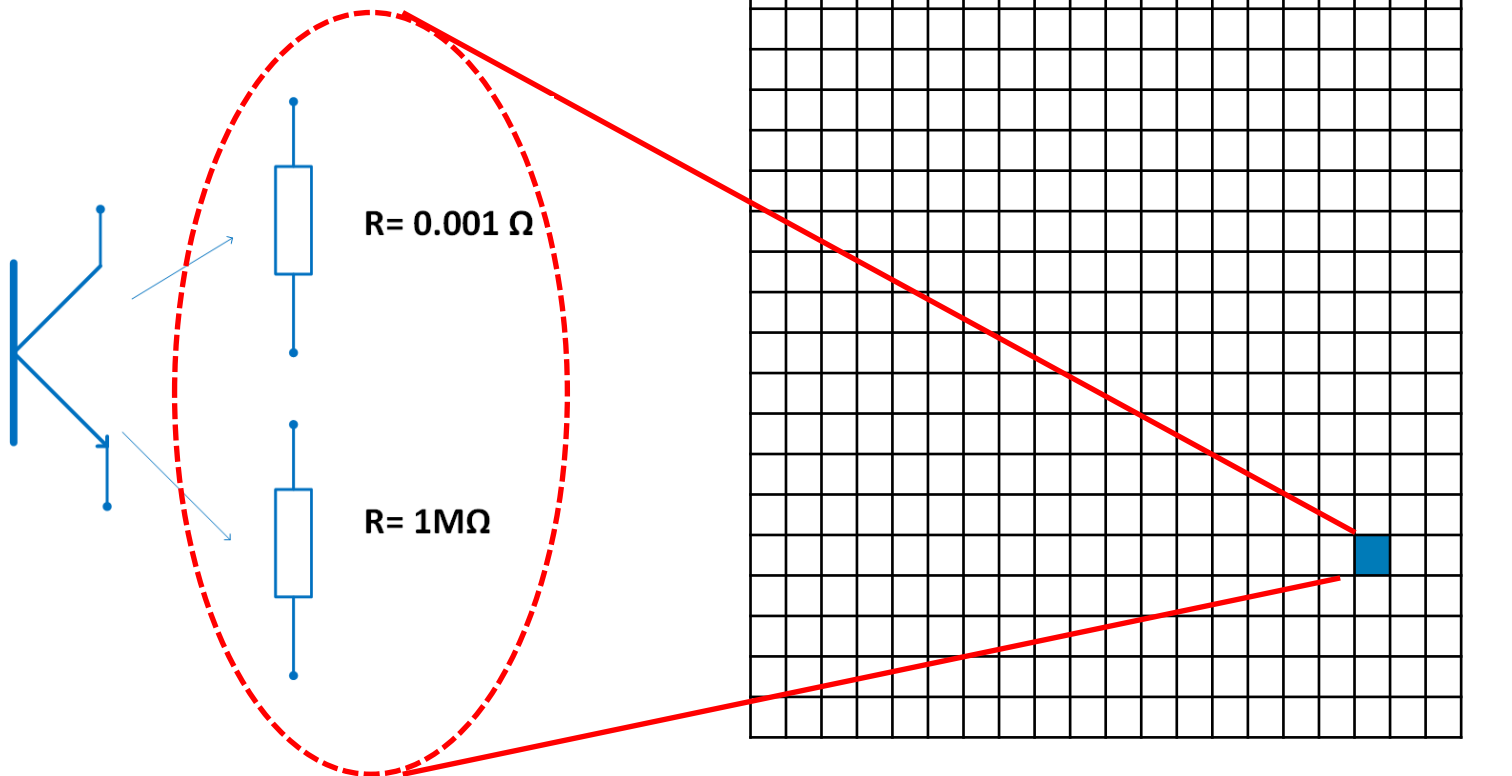
- Average model uses reference waveform in source. Fine details of switching events are lost
- Detailed model uses full PWM signal in source. Fine details of switching events are accurately modelled.
- Note: time step in detailed model must be small enough.

Average Model



Detailed model

- Two state switches
- CPU time demanding

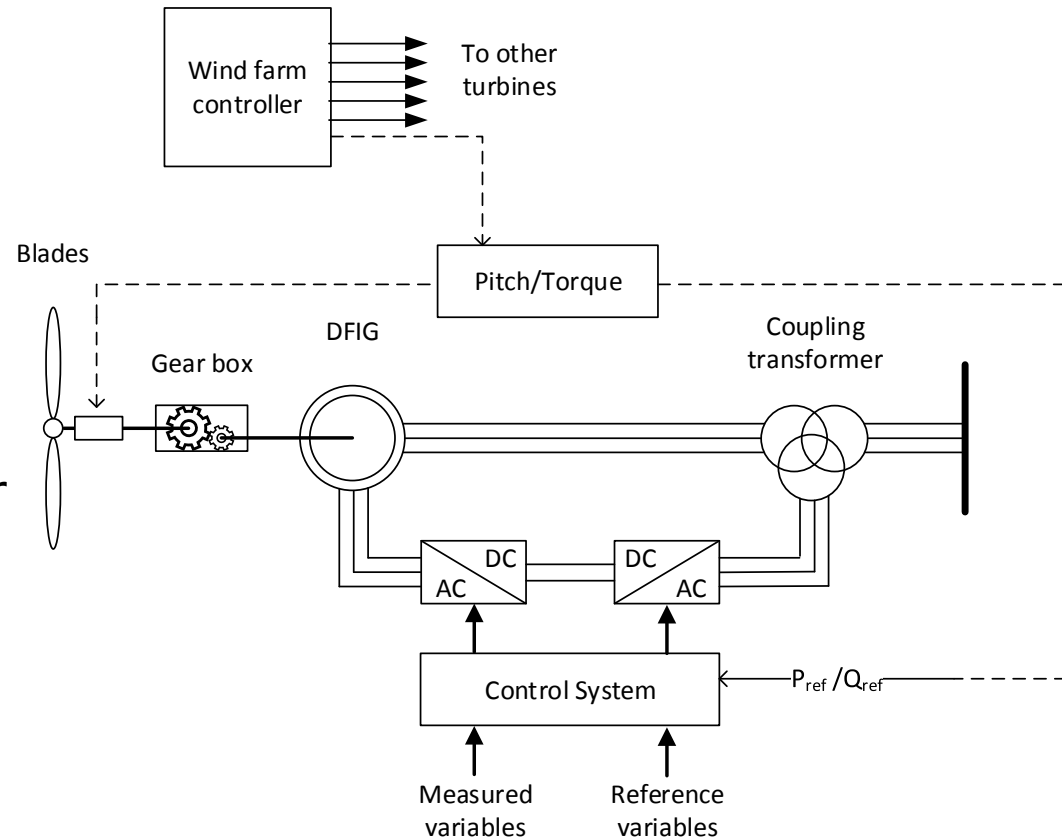


- Discuss the following generic models:
 - Type 3 wind turbine.
 - Type 4 wind turbine.
 - PV inverter.

Type 3 Turbine

EMT Type 3 Turbine

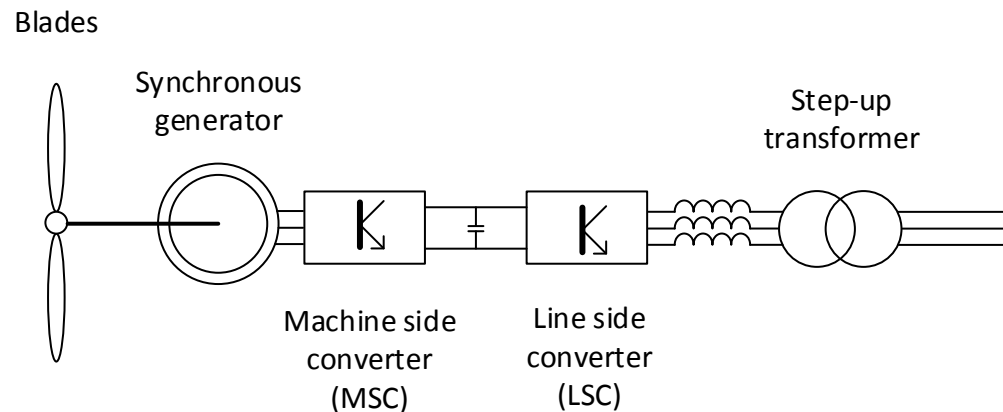
- Induction generator
- Back-to-back converter
 - Average or detailed
- Control system
 - V_{DC}
 - Active and reactive power
- Aerodynamic and drive train
 - 2-mass system
- Pitch and torque/power control
- Wind farm controller (slow)
 - P_{ref} and Q_{ref}



Type 4 Turbine

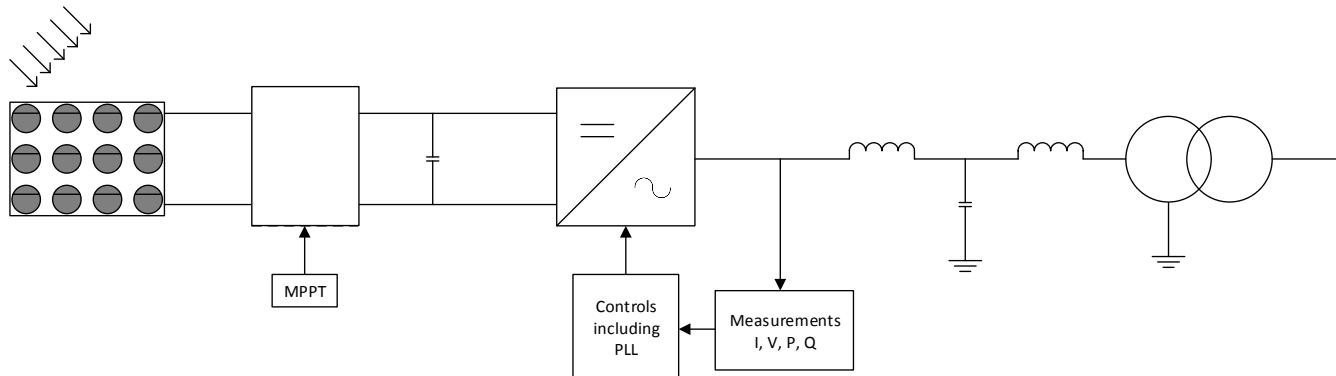
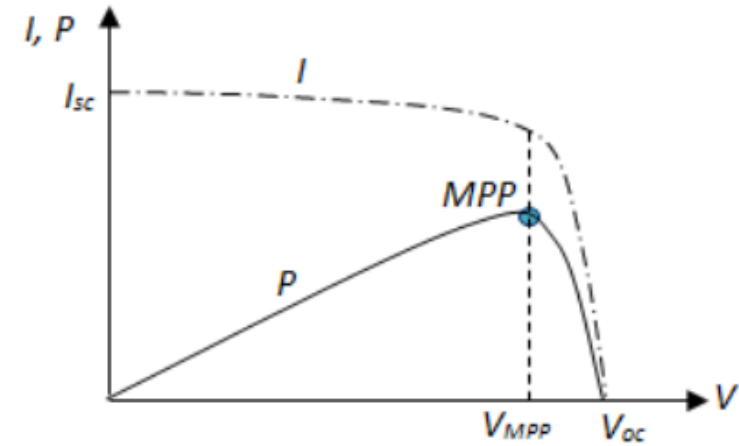
Type 4 wind farm

- PM synchronous generator
- Direct back-to-back converter
 - Average or detailed
 - MSC can be replaced by current source (if electro-mechanical behavior is not required. E.g. wind variation tests)
- Not shown: pitch/torque controller, wind farm controller



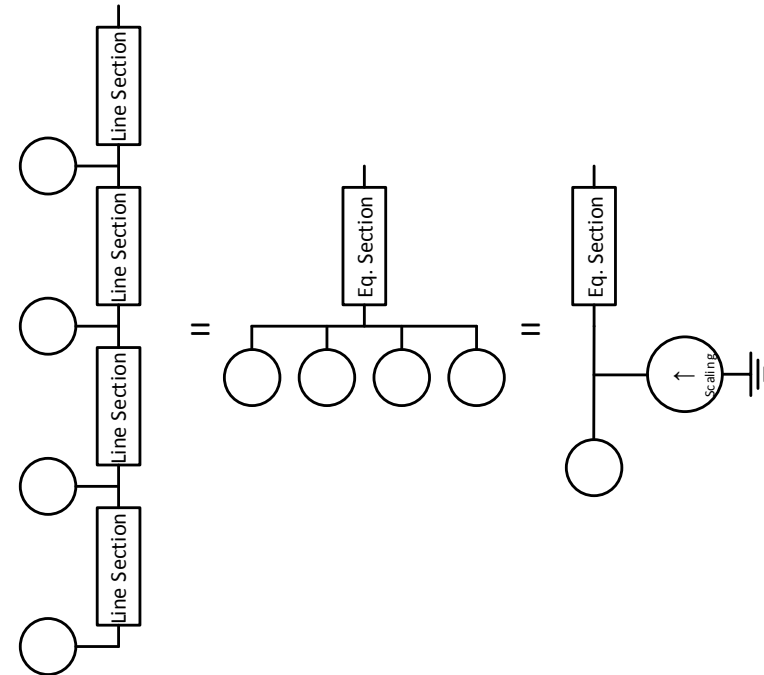
PV inverter

- Similar to type 4 converter (from AC onwards)
- MPPT



Wind farm/PV Solar farm aggregation

- Computationally demanding simulate full collector network with many detailed models.
Answer: aggregate.
- Steps to aggregate:
 1. Make equivalent line section
 2. Scale current N times



- Several methods make equivalent line section

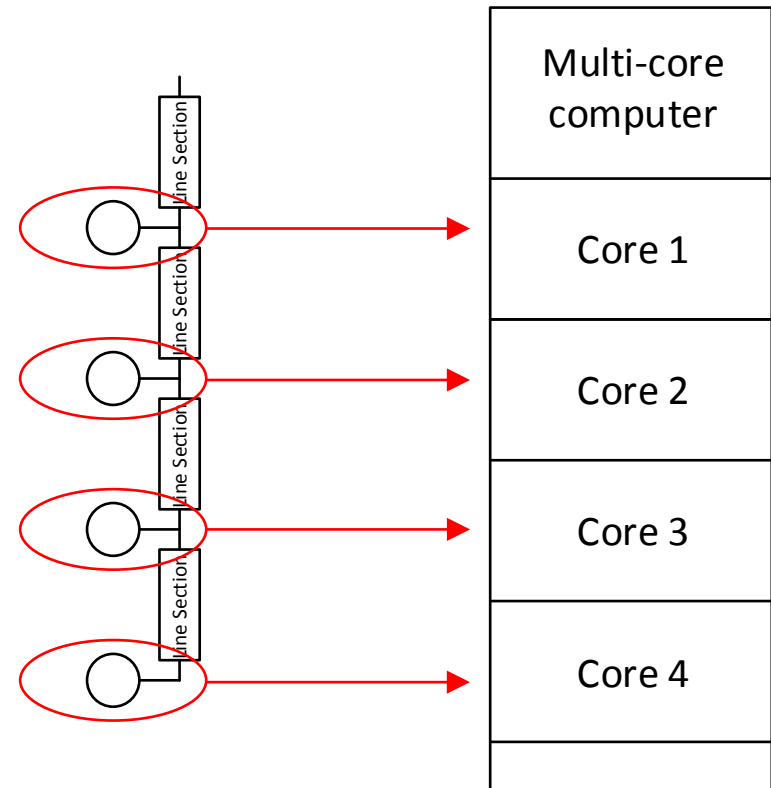
Ref. 1: *Equivalencing the collector system of a large wind power plant*, Muljadi et. al

Ref. 2: *Efficient EMT modeling approach to studying resonance phenomenon in PV and wind energy systems*, Pielahn, Mudunkotuwa, Ranaweera, Muthumuni

Parallel Processing - ENI

- If full details of feeder branches are needed -> can't aggregate
 - May have to run all or a large part of the collector network
- Allocate each converter model of the collector network onto a separate core on machine (Electric Network Interface)
- Also possible to split the simulation onto several computers separated by distance

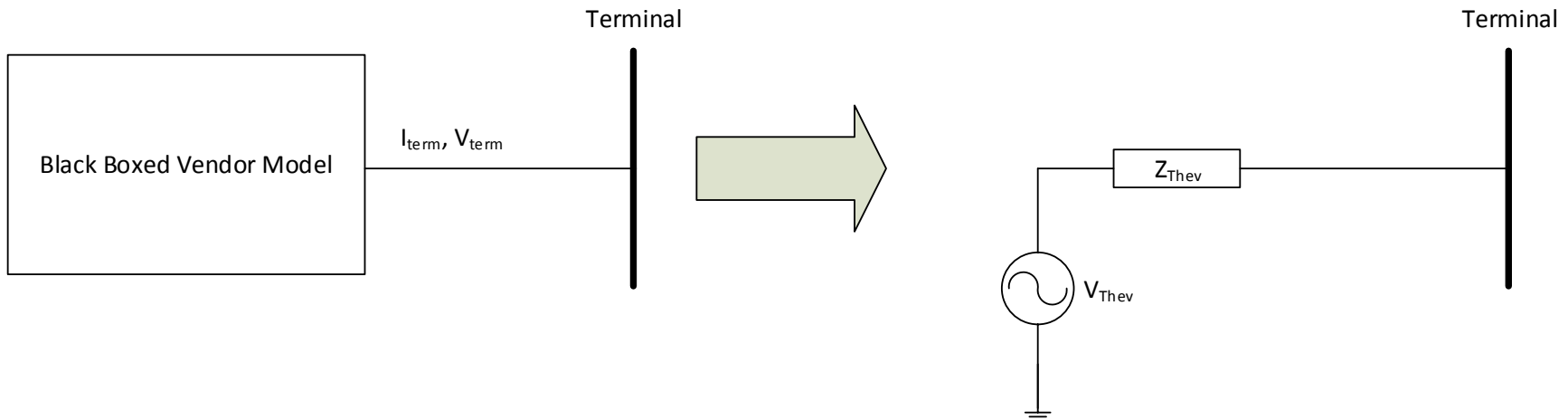
Note: ENI does not cause inaccuracies or time step delays.



Harmonic Model Derivation

Harmonic Model Derivation

- What is a harmonic model?
 - Harmonic model represent the converter as a Thévenin equivalent source.
 - Thévenin equivalence is calculated for different harmonics.

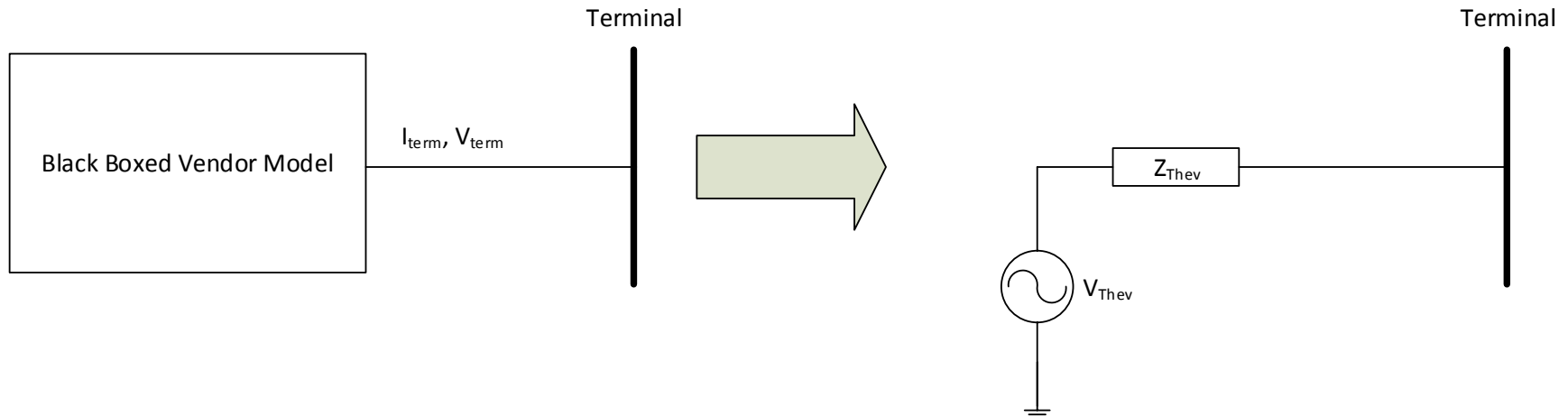


- Why we need harmonic model?
 - To calculate the total harmonic distortion of a renewable farm at the point of interconnection (POI)
 - Utility interest to know the impact upon interconnection of renewable farm.
 - Harmonic model used in harmonic analysis tools.

Harmonic Model Derivation

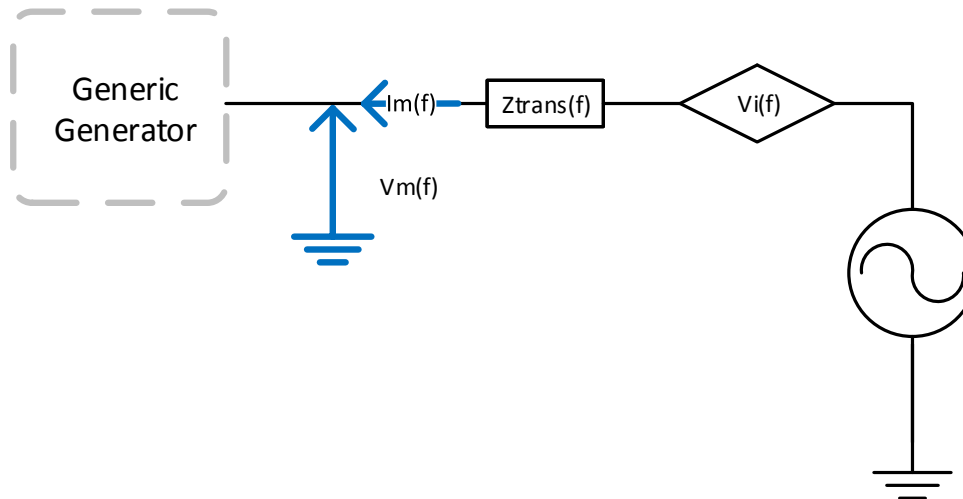
- Generally the harmonic model is a table. E.g.

Harmonic order	$ V_{thev} $	$Ph(V_{thev})$	$ Z_{thev} $	$Ph(Z_{thev})$
1	X	X	X	X
2	X	X	X	X
...
19	X	X	X	X
20	X	X	X	X



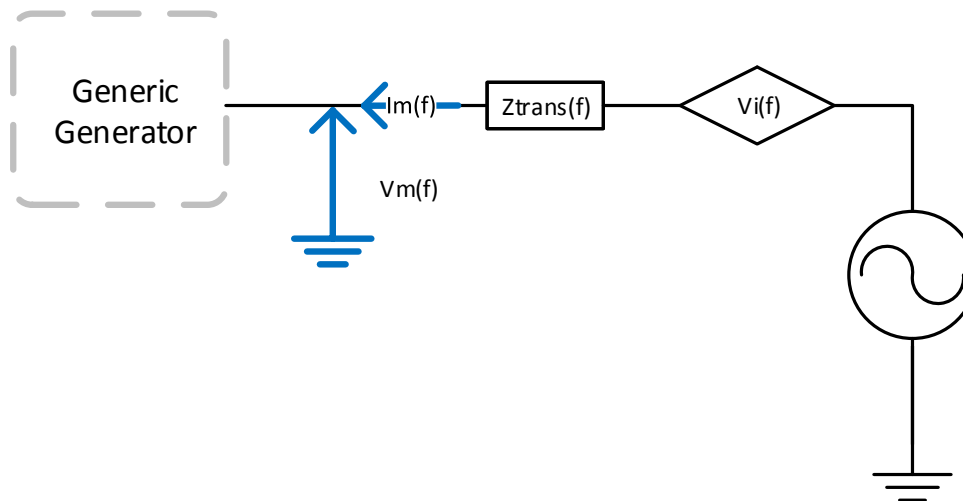
Harmonic Model Derivation

- Converter model is black boxed, provided by vendor
- Only known quantities are the terminal harmonic measurements:
 $I_m(f)$, $V_m(f)$
- Question: how to determine Thévenin equivalence using only these terminal values?
- Question: $I_m(f)$ and $V_m(f)$ are very small -> How to measure them?



Harmonic Model Derivation

- Answer: External excitations are needed
 - Harmonic voltage source is connected in series $V_i(f)$
- The magnitude of $V_i(f)$ are determined experimentally. Typically they should be a few % of the fundamental grid voltage.



Harmonic Model Derivation

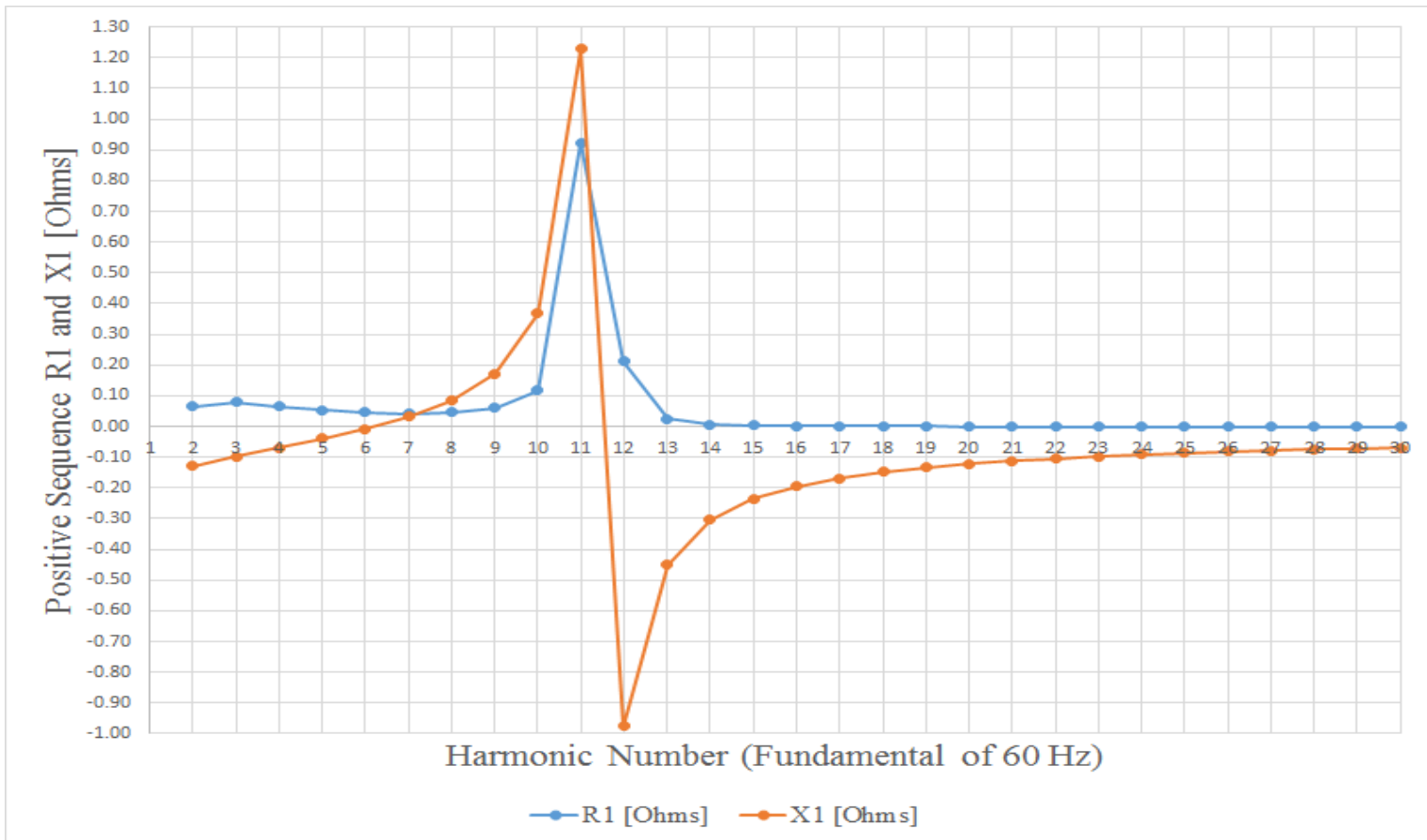
- To calculate the impedance $Z(f)$ at the terminal, inject excitation voltages at the same frequency.
- Measure terminal voltage and current. Repeat with a slightly modified voltage injection
 - $V_1(f), I_1(f), V_2(f), I_2(f) \rightarrow$ phasors

$$Z_{th}(f) = \frac{V_2(f) - V_1(f)}{I_2(f) - I_1(f)}$$

$$V_{th}(f) = -I_1(f) \cdot Z_{th}(f) + V_1(f)$$

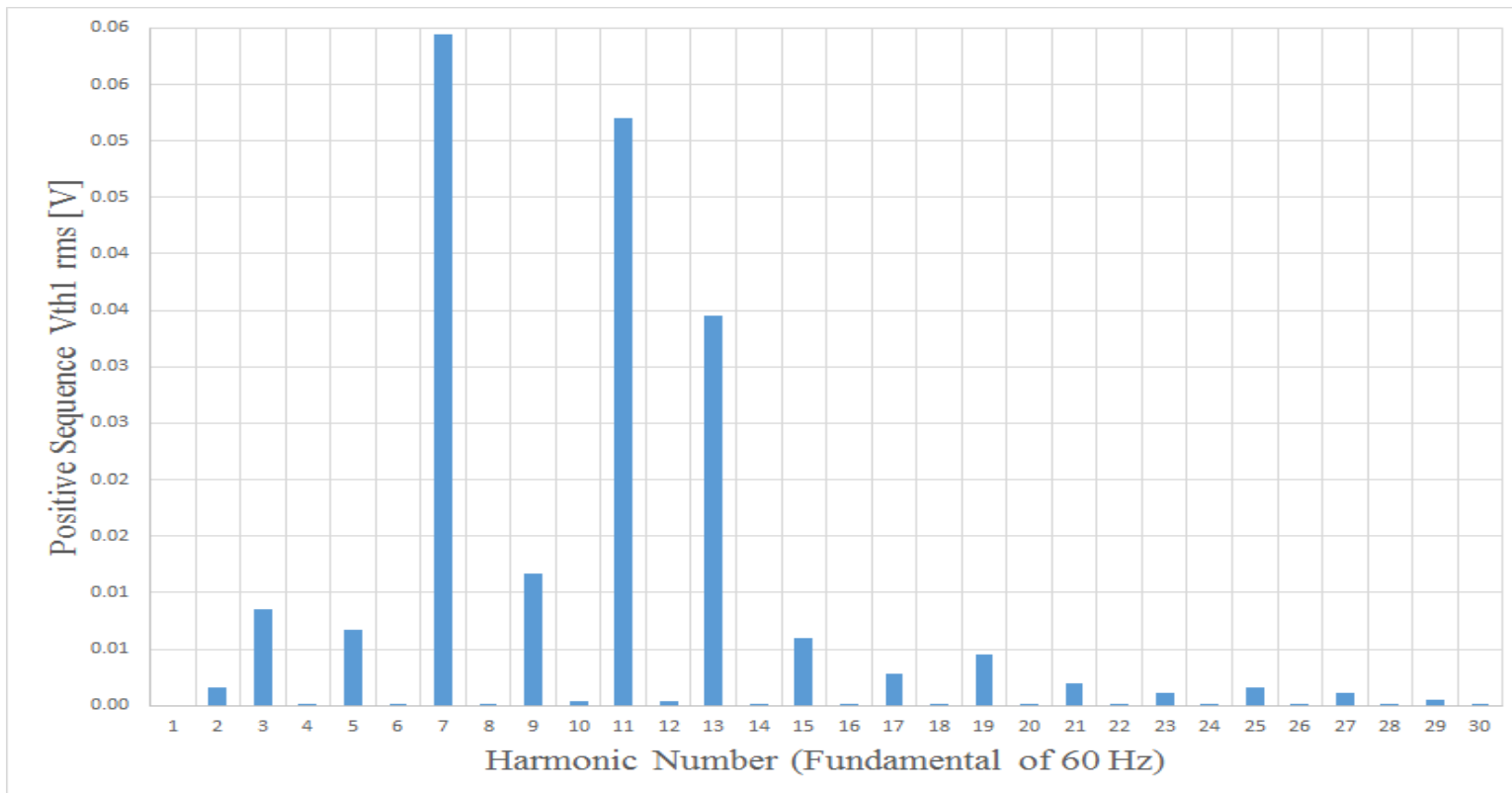
Harmonic Model Derivation

- Typical results...



Harmonic Model Derivation

- Typical results...



Harmonic Model Derivation

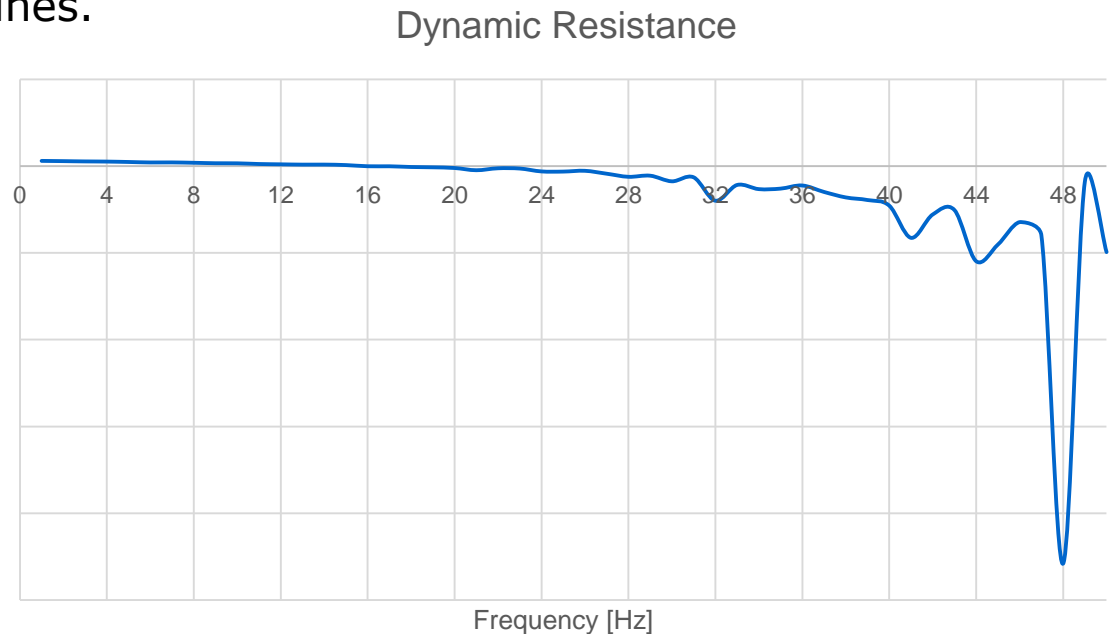
- Practical application has more than one equivalent harmonic model (collector network).
- The fundamental Thévenin angle of the harmonic model is in reference to the phase angle of converter terminal voltage. If voltage angle changes by $\Delta\varphi$, then fundamental Thévenin angle must change by the same amount. (maintain power flow)
- E.g. if the fundamental voltage angle is changed by an amount $\Delta\varphi$, then the angles of the harmonic model must be shifted by

$$\angle V_{th_shifted}(f) = \angle V_{th}(f) + n \cdot \Delta\varphi$$

where n is the harmonic number.

Harmonic Model Derivation

- What about dynamic resistance?
- $Z(f) = \frac{v(f)}{i(f)}$
- The real part of the Thévenin impedance is called *Dynamic Resistance*.
- Used to screen for negative frequency region in which converter amplifies harmonics.
- Predominant in type 3 turbines.



Thank you