

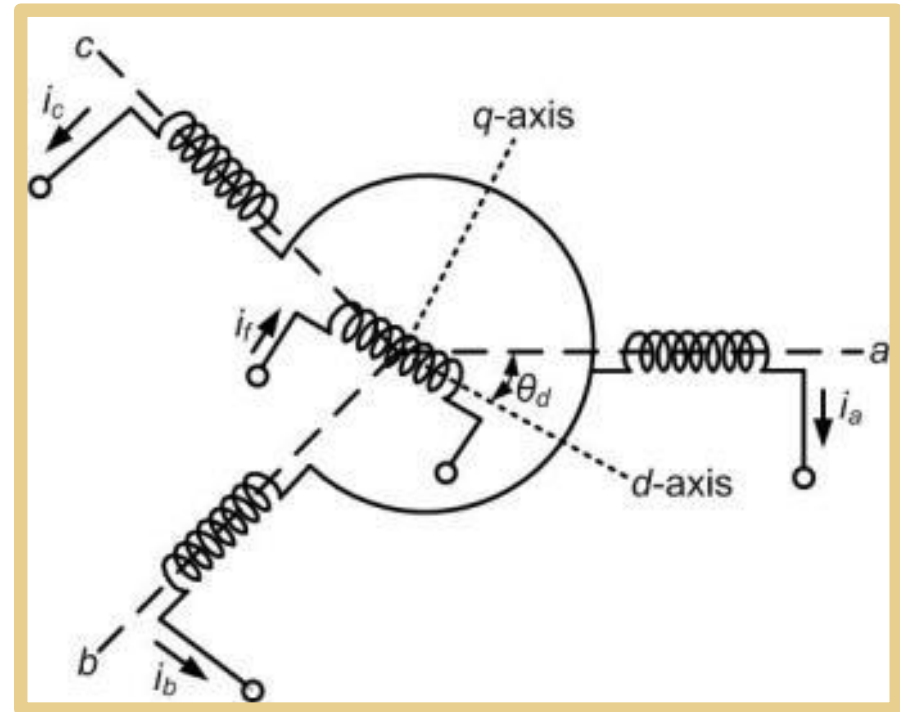


# Machine Modeling and Power System Study Applications

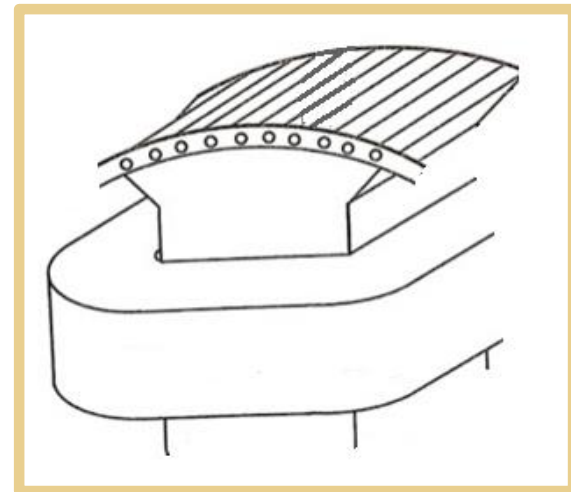
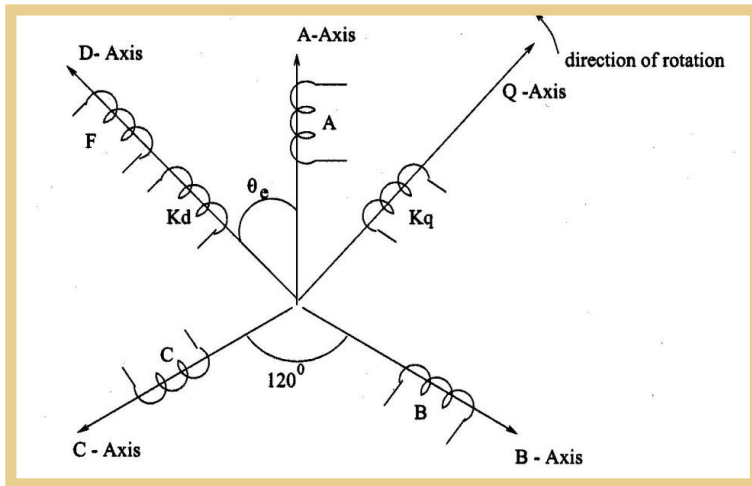
Presented by: Dharshana Muthumuni



- Mathematical representation of machine windings and rotor dynamics
- Machine models and controls models available in PSCAD
- Setting up a PSCAD simulation case
  - Synchronous machine (initialization of machine and control models)
  - Induction machine (starting example)
- Illustration of Simulation examples
  - Model setup and data entry and model response
  - Model Benchmarking
  - Black start restoration studies
  - Voltage flicker due to compressor load driven by a synchronous machine
  - **Sub synchronous resonance and torsional interactions**
  - Voltage dips due to induction motor starting and mitigation options
  - Applications in wind generation (DFIG)

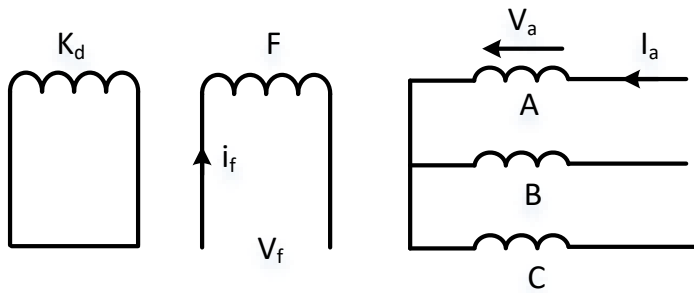


Representation of the machine coils and the direction of their magnetic axes

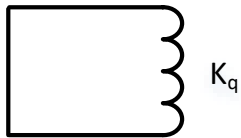


$$[V] = [R][i] + \frac{d}{dt} ([L][i])$$





$$[V] = [R][i] + \frac{d}{dt}([L][i])$$



$$R := \begin{bmatrix} R_s & 0 & 0 & 0 & 0 & 0 \\ 0 & R_s & 0 & 0 & 0 & 0 \\ 0 & 0 & R_s & 0 & 0 & 0 \\ 0 & 0 & 0 & R_f & 0 & 0 \\ 0 & 0 & 0 & 0 & R_{kd} & 0 \\ 0 & 0 & 0 & 0 & 0 & R_{kq} \end{bmatrix}$$

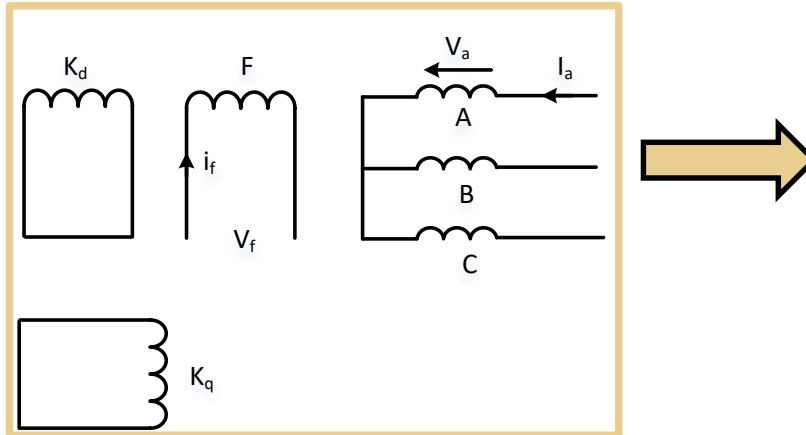
$$L := \begin{bmatrix} L_a & M_{ab} & M_{ac} & M_{af} & M_{akd} & M_{akq} \\ M_{ab} & L_b & M_{bc} & M_{bf} & M_{bkd} & M_{bkq} \\ M_{ac} & M_{bc} & L_c & M_{cf} & M_{ckd} & M_{ckq} \\ M_{af} & M_{bf} & M_{cf} & L_f & M_{fkd} & M_{fkq} \\ M_{akd} & M_{bkd} & M_{ckd} & M_{fkd} & L_{kd} & 0 \\ M_{akq} & M_{bkq} & M_{ckq} & 0 & 0 & L_{kq} \end{bmatrix}$$

Position dependent (time dependent) elements.



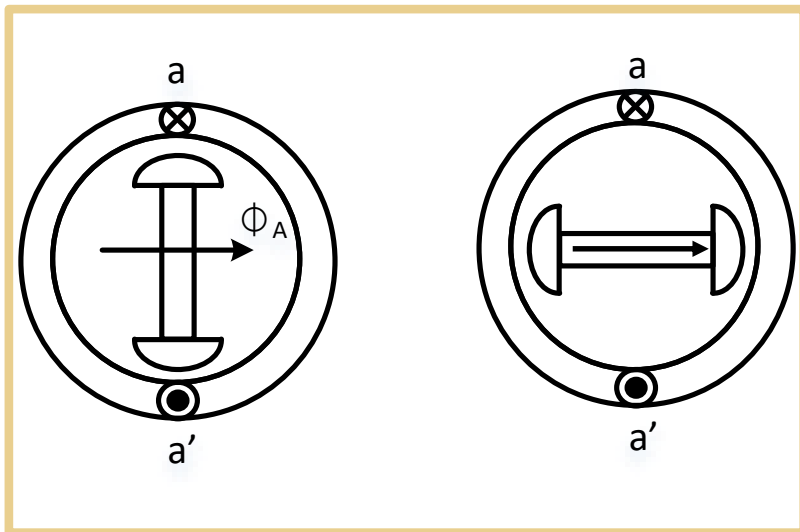
$$L_a = (L_1 + L_2) + L_3 \cos(2\theta)$$

$$M_{af} = M_f \cos(2\theta)$$



$$[V] = [R][i] + \frac{d}{dt}([L][i])$$

$$L := \begin{bmatrix} L_a & M_{ab} & M_{ac} & M_{af} & M_{akd} & M_{akq} \\ M_{ab} & L_b & M_{bc} & M_{bf} & M_{bkd} & M_{bkq} \\ M_{ac} & M_{bc} & L_c & M_{cf} & M_{ckd} & M_{ckq} \\ M_{af} & M_{bf} & M_{cf} & L_f & M_{fkd} & M_{fkq} \\ M_{akd} & M_{bkd} & M_{ckd} & M_{fkd} & L_{kd} & 0 \\ M_{akq} & M_{bkq} & M_{ckq} & 0 & 0 & L_{kq} \end{bmatrix}$$



Position dependent (time dependent) elements of Inductance matrix

$$L_a = (L_1 + L_2) + L_3 \cos(2\theta)$$

$$M_{af} = M_f \cos(2\theta)$$

## Stator Side

$$V_d = R_s \cdot i_d + \frac{d}{dt} \lambda_d(t) - \lambda_q(t) \cdot \omega_r$$

$$V_q = R_s \cdot i_q + \frac{d}{dt} \lambda_q(t) + \lambda_d(t) \cdot \omega_r$$

$$V_0 = R_0 \cdot i_0 + \frac{d}{dt} \lambda_0(t)$$

## Rotor Side

$$E_f = R_f \cdot i_f + \frac{d}{dt} \lambda_f(t)$$

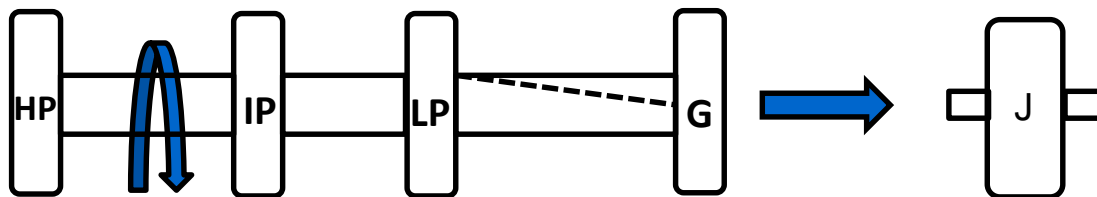
$$0 = R_{kd} \cdot i_{kd} + \frac{d}{dt} \lambda_{kd}(t)$$

$$0 = R_{kq1} \cdot i_{kq1} + \frac{d}{dt} \lambda_{kq1}(t)$$

$$0 = R_{kq2} \cdot i_{kq2} + \frac{d}{dt} \lambda_{kq2}(t)$$

Dampers – 2 on Q-axis

## Mechanical rotation



Speed -  $\omega_k$

$$T_m - T_e = J \frac{d\omega}{dt} + B\omega$$

Parameter	
Stator leakage Inductance	$X_l$
Synchronous Reactance	$X_d$
	$X_q$
Transient Reactance	$X'_d$
	$X'_q$
Sub transient Reactance	$X''_d$
	$X''_q$
Transient OC Time Constant	$T'_{do}$
	$T'_{qp}$
Sub transient OC Time Constant	$T''_{do}$
	$T''_{qp}$

[ABC]  $\longrightarrow$  [dq0]

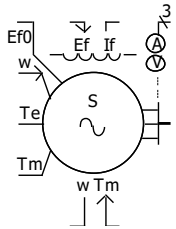
Direct linear relationship

$\longrightarrow$   $L_a, L_b, \dots, M_{ab}, \dots, L_f, M_{af}, L_{kd}, \dots$

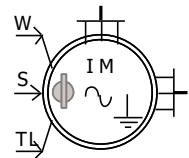
Examples:

Field open time constant:  $T'_{d0} = \frac{L_f}{R_f}$

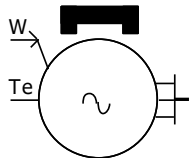




Synchronous Machine



Induction Machine

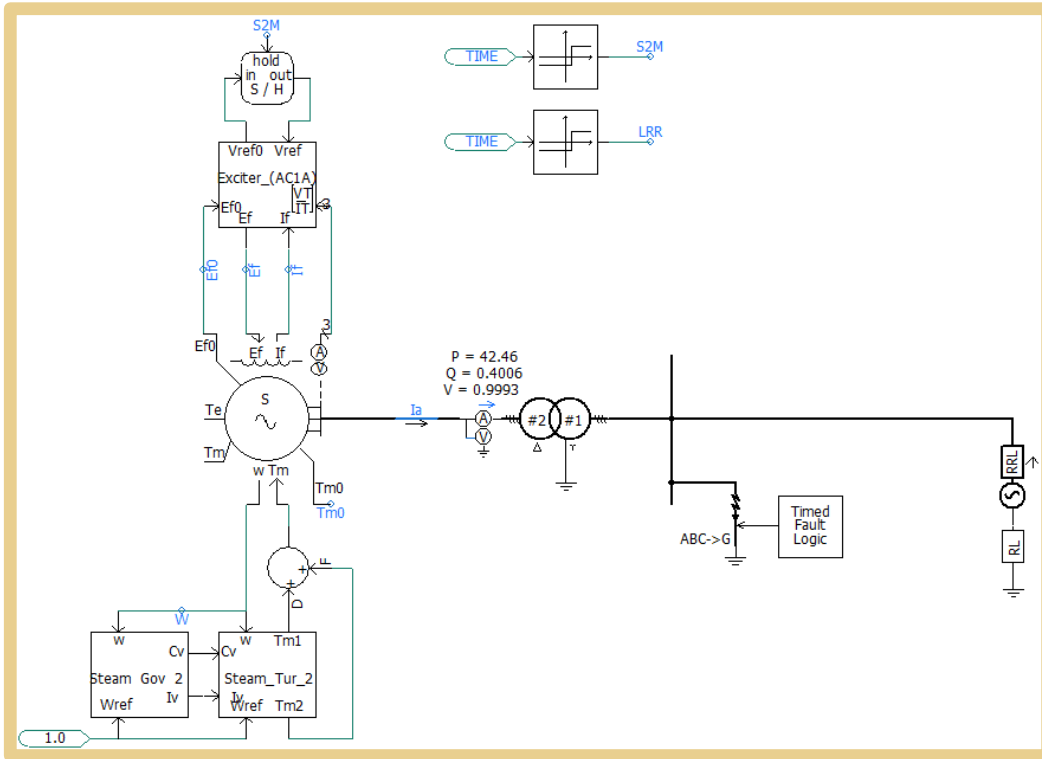


Permanent Magnet Machine

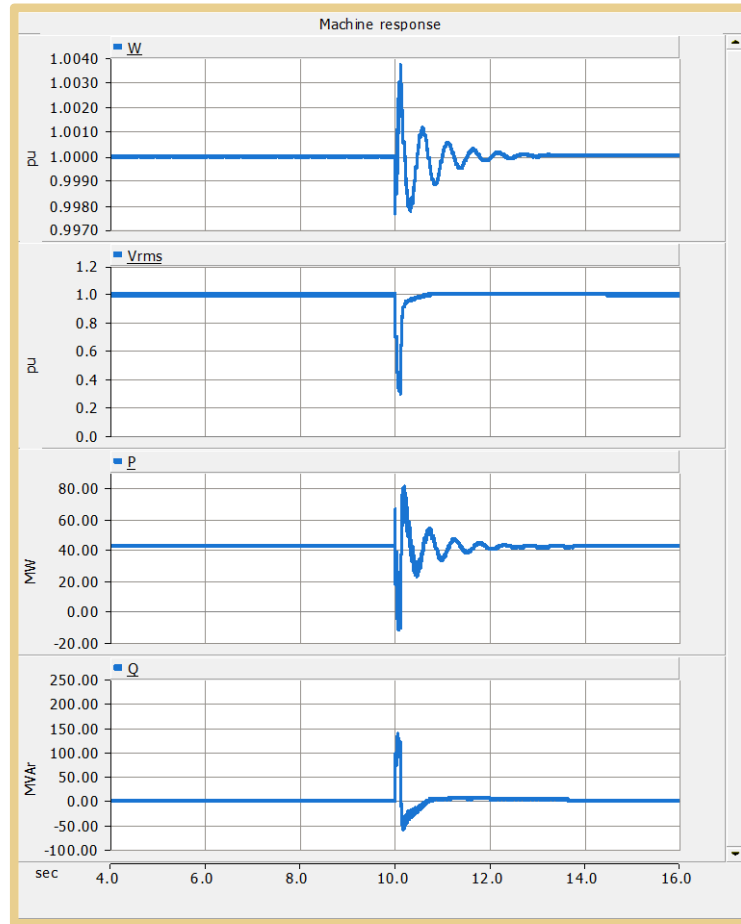
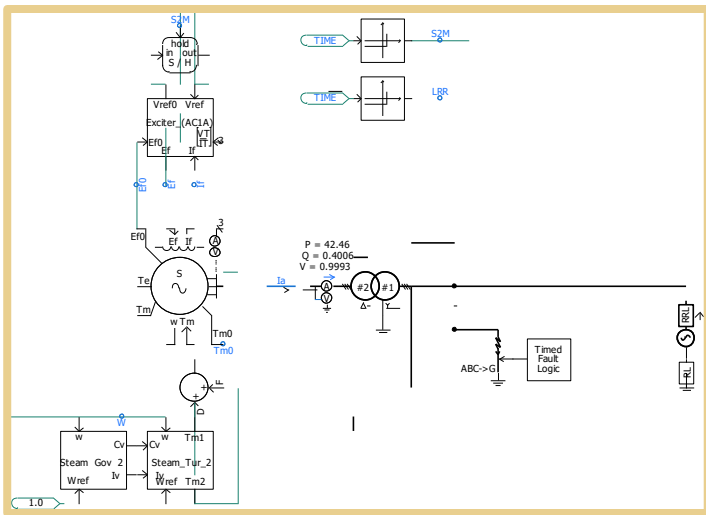
PSCAD Machine models are accurate and reliable.

- In use for over 30 years
- Almost all major power system projects (HVDC, large generation) were studied using these models
- In recent times, the wind turbine models of all vendors use PSCAD machine models





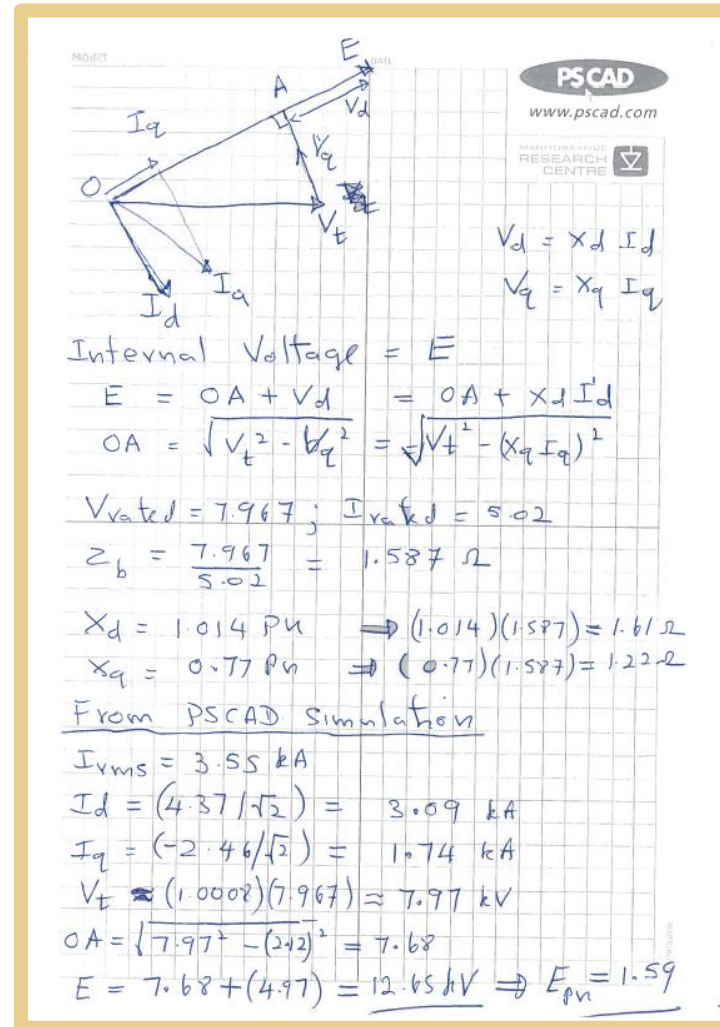
Parameter		Thermal Units (Typical values)
Stator leakage Inductance	$X_l$	0.1-0.2
	$X_d$	1.0-2.3
Synchronous reactance	$X_q$	1.0-2.3
	$X'_d$	0.15-0.4
Transient Reactance	$X'_q$	0.3-1.0
	$X''_d$	0.12-0.25
Subtransient Reactance	$X''_q$	0.12-0.25
	$T'_{do}$	3.0-10.0 s
Transient OC time constant	$T'_{qo}$	0.5-2.0 s
	$T''_{do}$	0.02-0.05 s
Subtransient OC Time constant	$T''_{qo}$	0.02-0.05 s

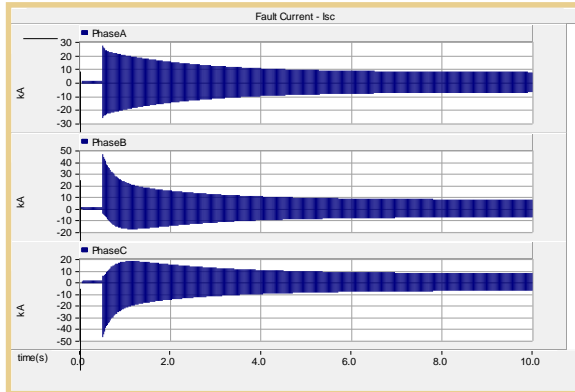


Technical note available on how to set up the machine model and controls.

## Steady state operation:

Hand calculations confirm PSCAD model response

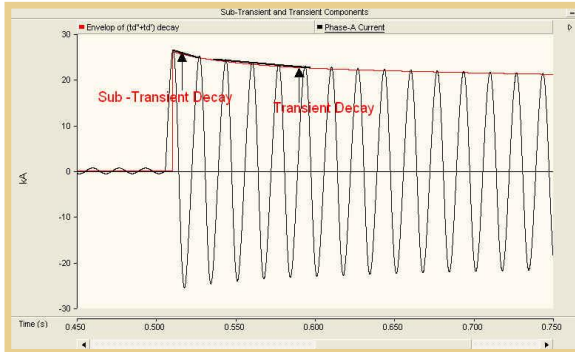




Transient response: PSCAD model follows expected response (see technical note)

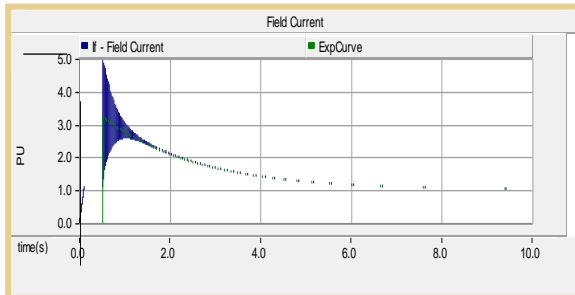
### Transient response

$$T_d' = \left( \frac{X_d}{X_d'} \right) \cdot T_{do} = \left( \frac{0.314}{1.014} \right) \cdot 6.55 = 2.03 \text{ s}$$



### Sub Transient response

$$T_d'' = \left( \frac{X_d}{X_d''} \right) \cdot T_{do} = \left( \frac{0.280}{0.314} \right) \cdot 0.039 = 34.7 \text{ ms}$$

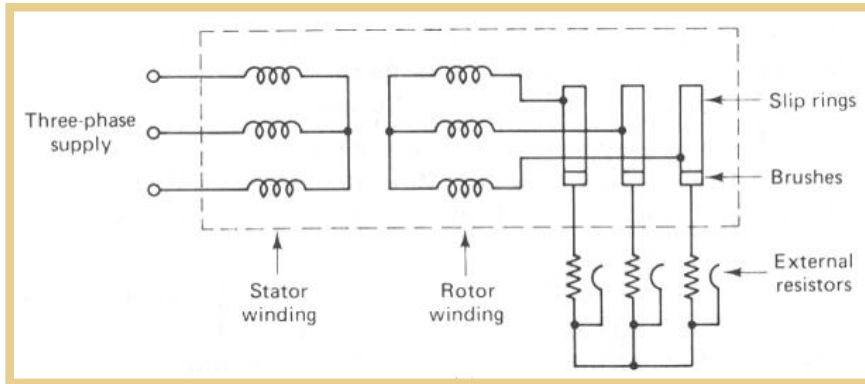


### Field current decay time constant

$$I_{fo}' = \left( \frac{X_d}{X_d'} \right) \cdot I_{fo} = \left( \frac{1.014}{0.314} \right) \cdot 1 = 3.23 \text{ PU}$$

$$I_f' = I_{fo}' + (I_{fo}' - I_{fo}) \cdot e^{-t/T_d'} = 1 + (3.23 - 1) \cdot e^{-t/T_d'}$$





Machine response can be represented in the form of six mutually coupled winding

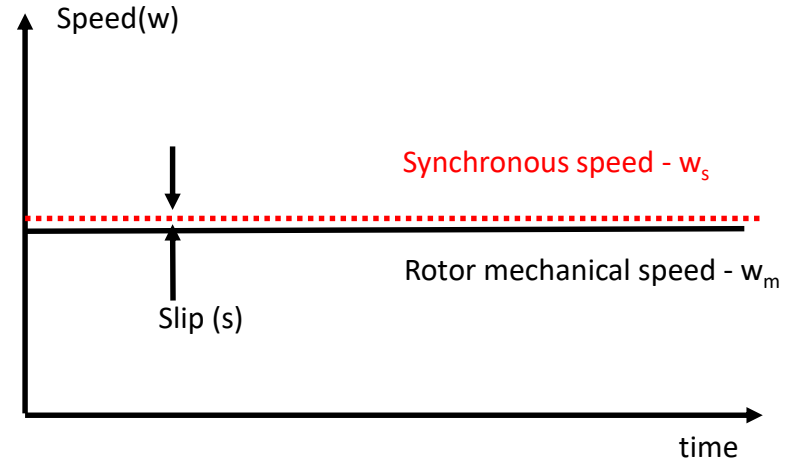
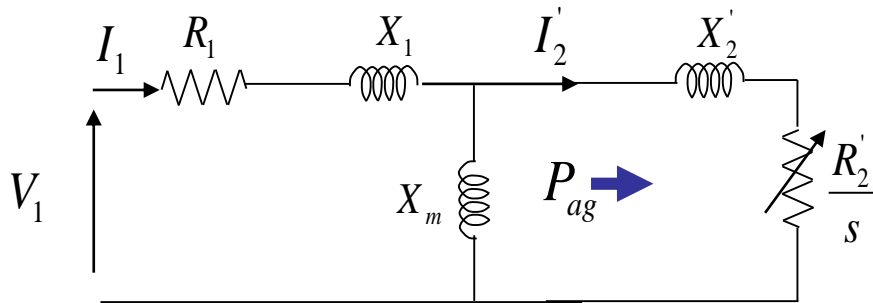
$$L_s = \begin{bmatrix} L_{ls} + L_{ms} & -.5L_{ms} & -.5L_{ms} \\ -.5L_{ms} & L_{ls} + L_{ms} & -.5L_{ms} \\ -.5L_{ms} & -.5L_{ms} & L_{ls} + L_{ms} \end{bmatrix}$$

$$L_r = \begin{bmatrix} L_{lr} + L_{mr} & -.5L_{mr} & -.5L_{mr} \\ -.5L_{mr} & L_{lr} + L_{mr} & -.5L_{mr} \\ -.5L_{mr} & -.5L_{mr} & L_{lr} + L_{mr} \end{bmatrix}$$

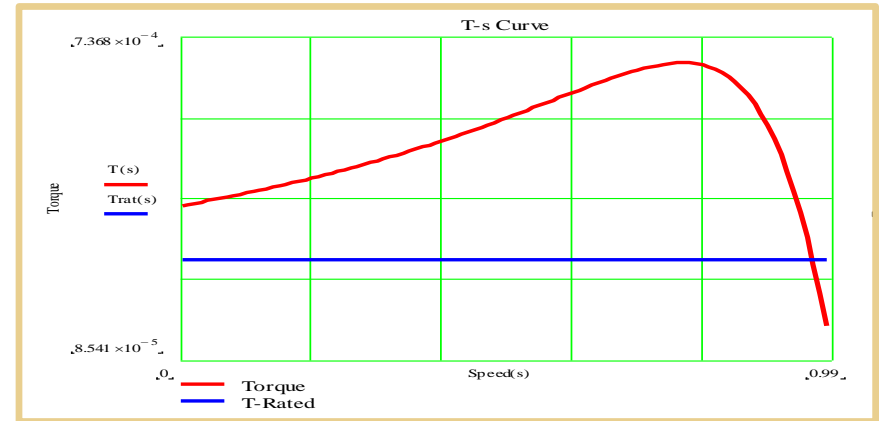
and

$$L_{sr} = 1_{sr} \begin{bmatrix} \cos\theta_r & \cos(\theta_r + \frac{2\pi}{3}) & \cos(\theta_r - \frac{2\pi}{3}) \\ \cos(\theta_r - \frac{2\pi}{3}) & \cos\theta_r & \cos(\theta_r + \frac{2\pi}{3}) \\ \cos(\theta_r + \frac{2\pi}{3}) & \cos(\theta_r - \frac{2\pi}{3}) & \cos(\theta_r) \end{bmatrix}$$

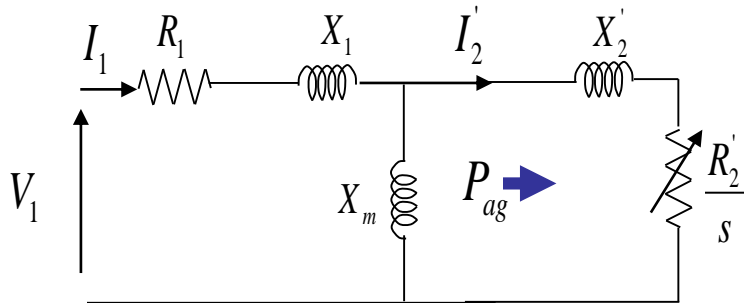
Steady state equivalent circuit and torque-slip characteristics



$$T(s) := \frac{3 \cdot V^2 \cdot R_2}{s \cdot w_0 \cdot \left[ \left( R_1 + \frac{R_2}{s} \right)^2 + (X_{eq})^2 \right]}$$

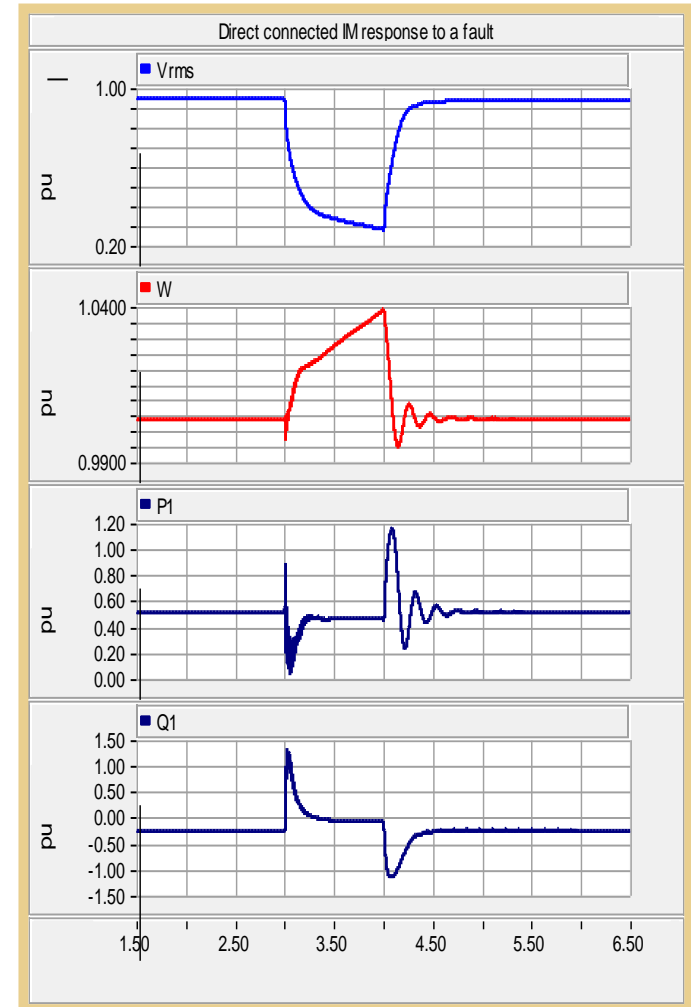


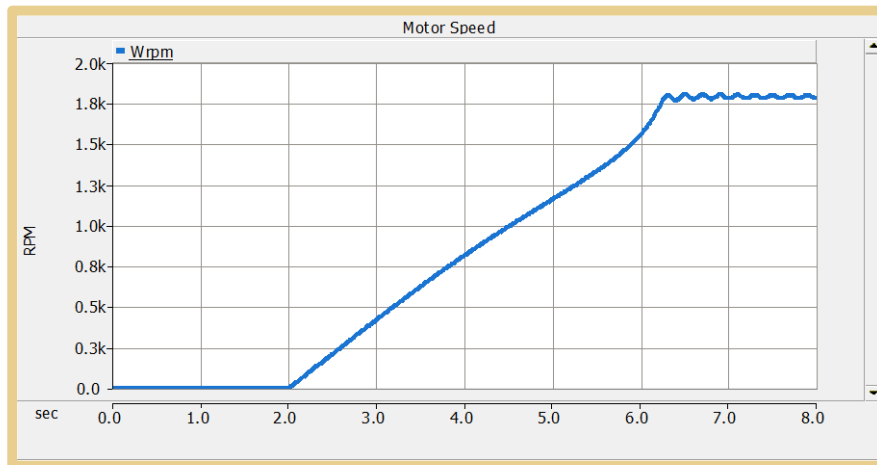
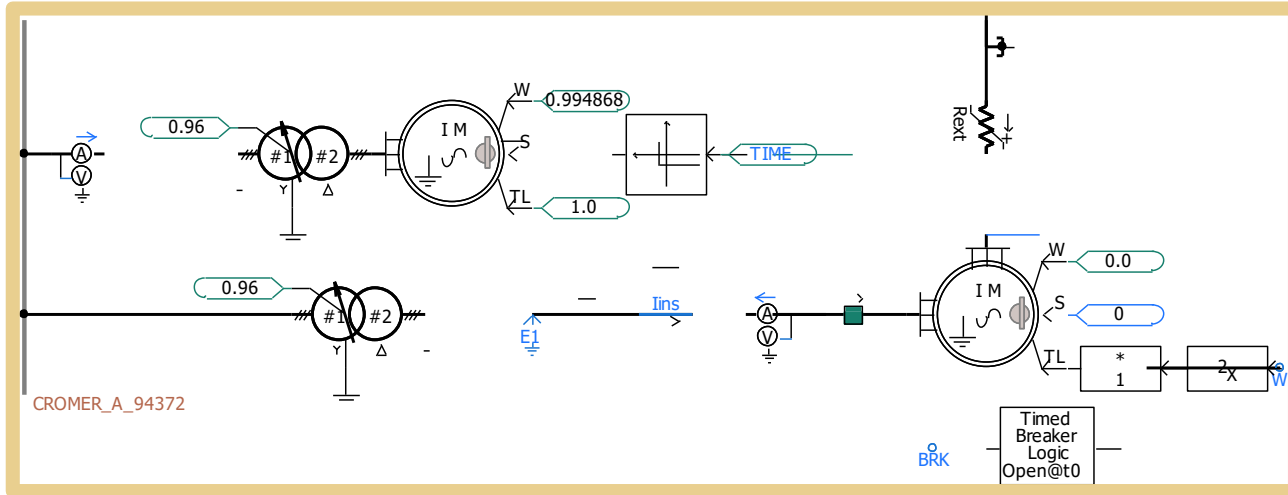
Induction machine response during fault recovery – High reactive power absorption can lead to voltage stability concerns



Machine speeds up (assume a Type 1 wind unit) during the fault

- At fault clearance, slip is larger (compared to normal operation)
- Stator and rotor current will be high as a result of high slip
- Increased reactive power absorption in leakage fields





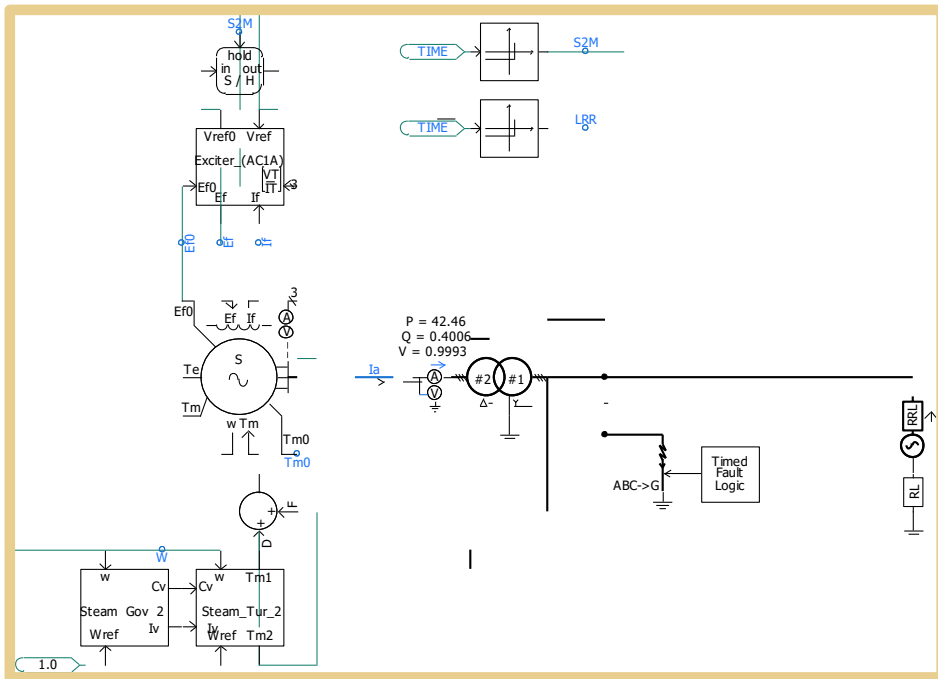
Technical note available on how to set up the machine model and controls

PSCAD

# Simulation examples

- Illustration of Simulation examples
  - Model setup and data entry
  - Model Benchmarking
  - Black start restoration studies
  - Voltage flicker due to compressor load driven by a synchronous machine
  - Sub synchronous resonance and torsional interactions
  - Voltage dips due to induction motor starting and mitigation options
  - Applications in wind generation (DFIG)





Synchronous Machine initialization and verification of response



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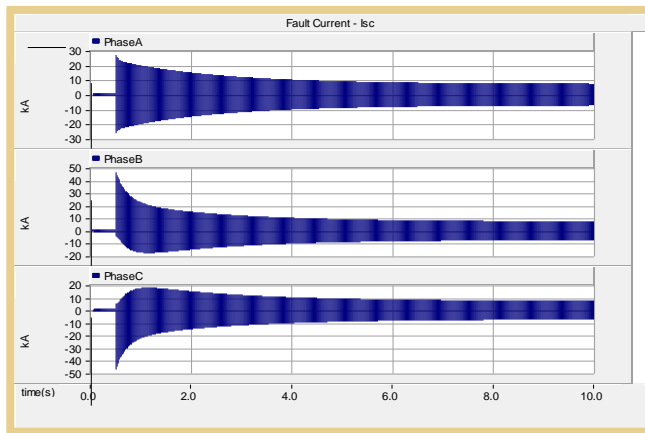
Transient response: PSCAD model follows expected response (see technical note)

Transient response

$$T_{d'} = \left( \frac{X_{d-}}{X_d} \right) \cdot T_{do-} = \left( \frac{0.314}{1.014} \right) \cdot 6.55 = 2.03 \text{ s}$$

Sub Transient response

$$T_{d''} = \left( \frac{X_{d-}}{X_{d-}} \right) \cdot T_{do-} = \left( \frac{0.280}{0.314} \right) \cdot 0.039 = 34.7 \text{ ms}$$



## Synchronous Machine – Short Circuit Test and Model Verification



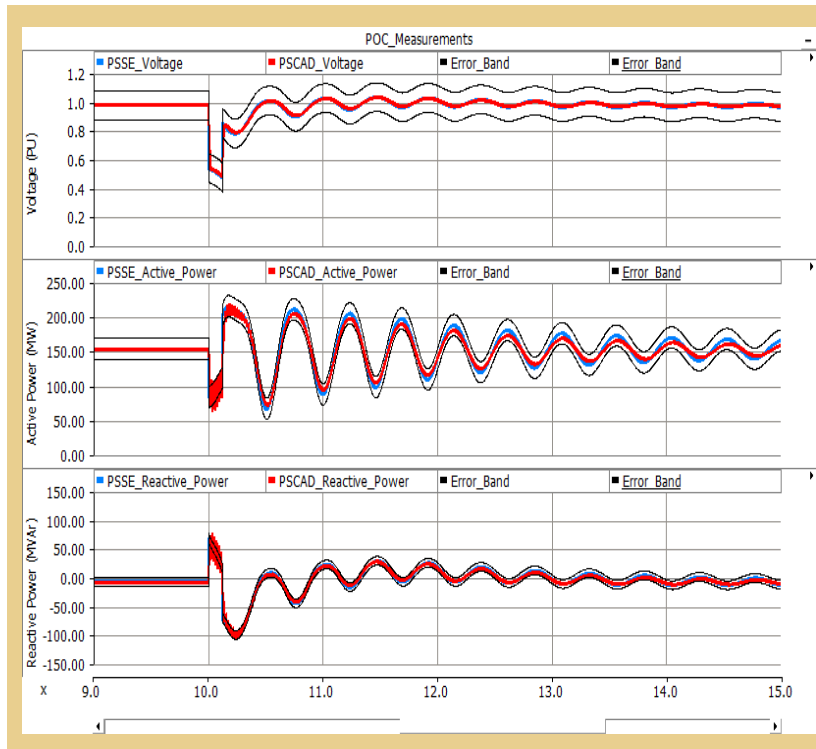
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Comparing response with RMS simulation results

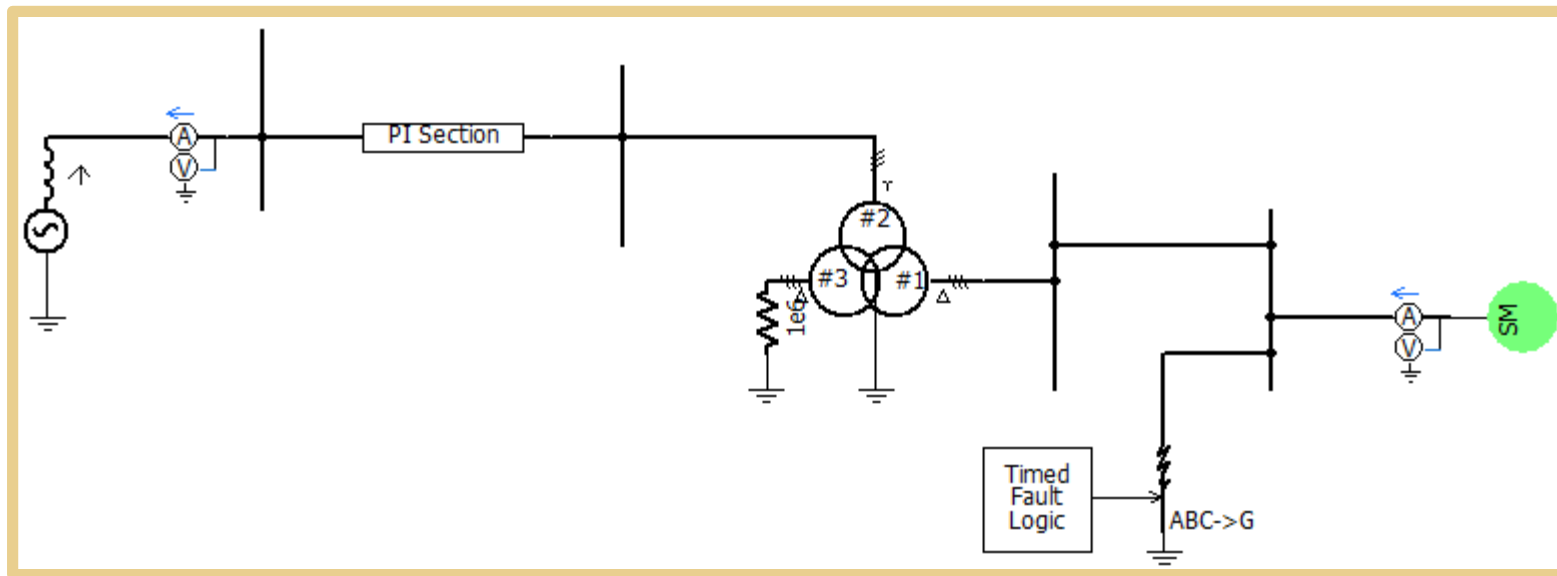
The results (even RMS quantities) are derived from two different methods of mathematical circuit solution techniques – There can be minor differences

## Synchronous generator fault ride through

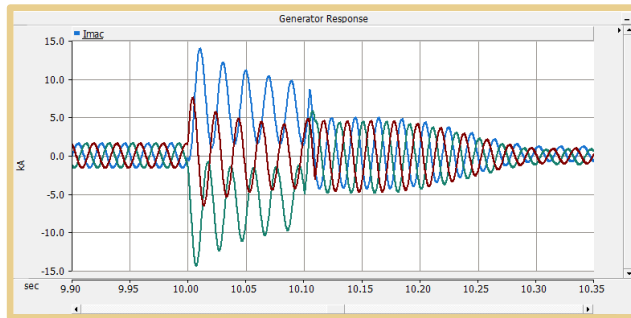
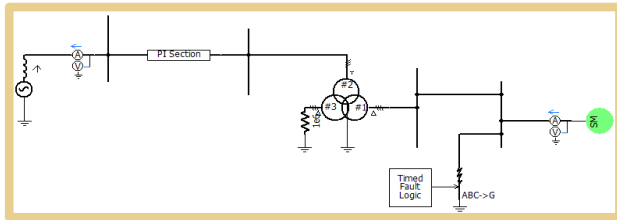


The results (even RMS quantities) are derived from two different methods of mathematical circuit solution techniques

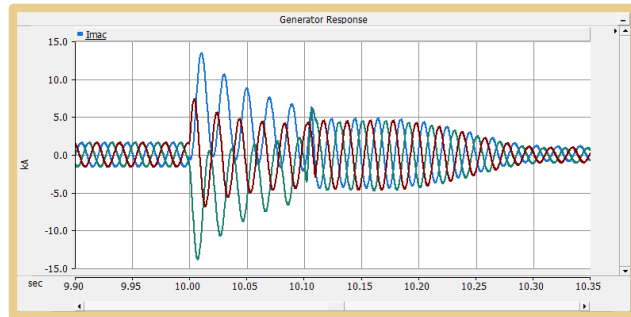
- The test circuits are simplified (ideal like)
- Note network dynamics such as DC offset in fault current
- In EMT, currents are interrupted at 'zero crossings'



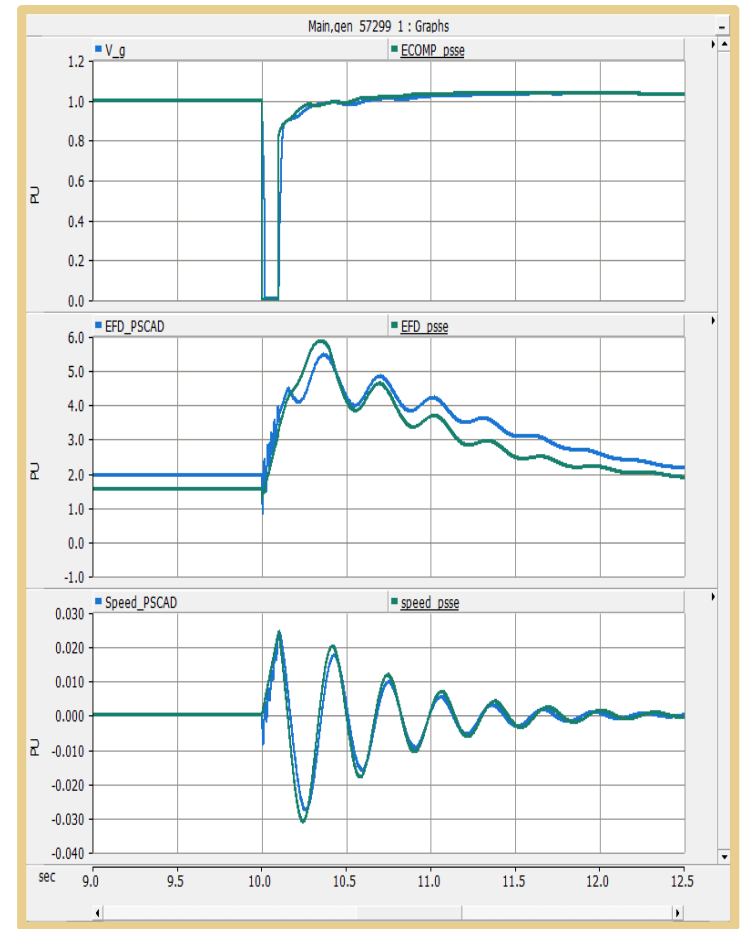
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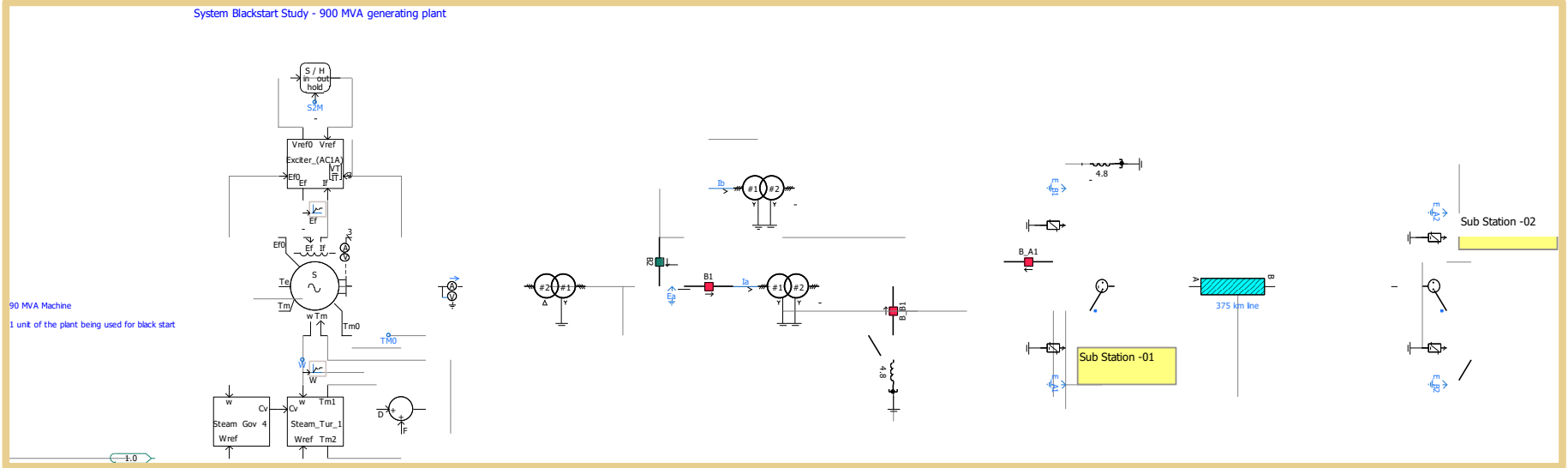
Zero fault resistance



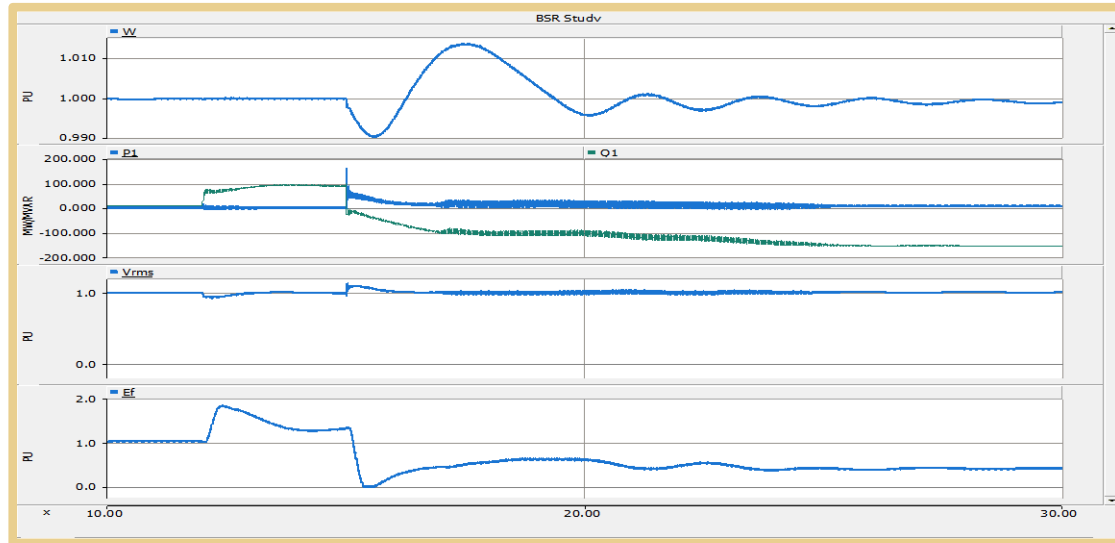
Low fault resistance



System Blackstart Study - 900 MVA generating plant

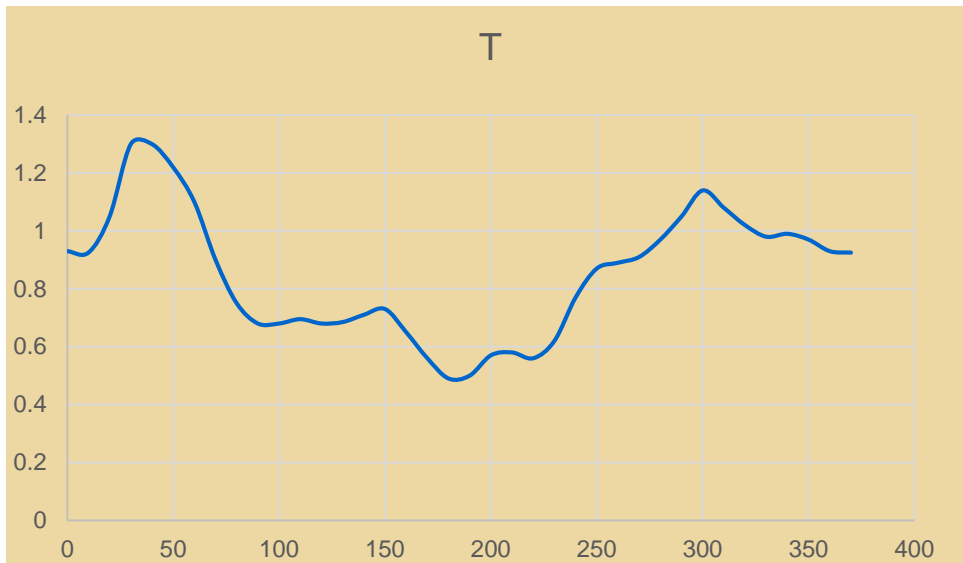


Example: Self Excitation  
when energizing a long line

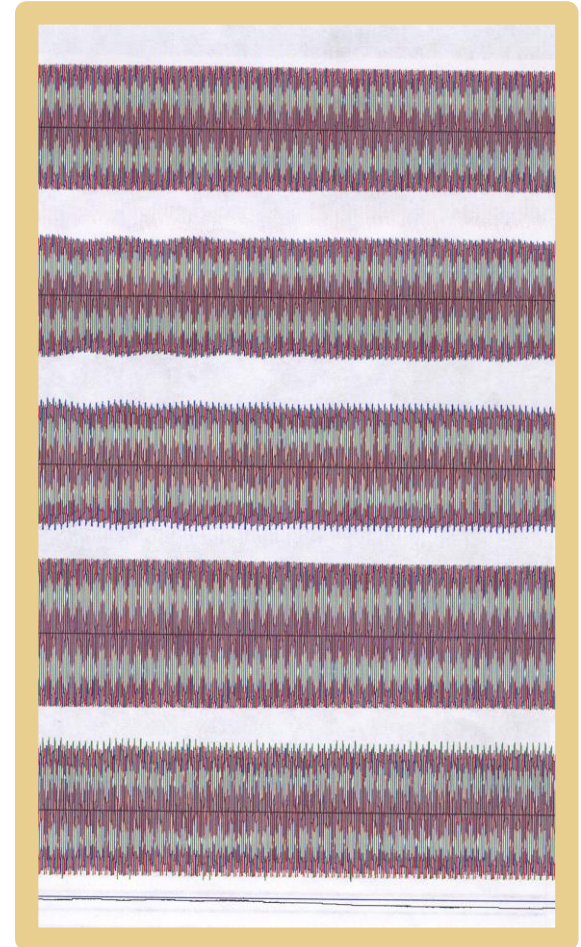


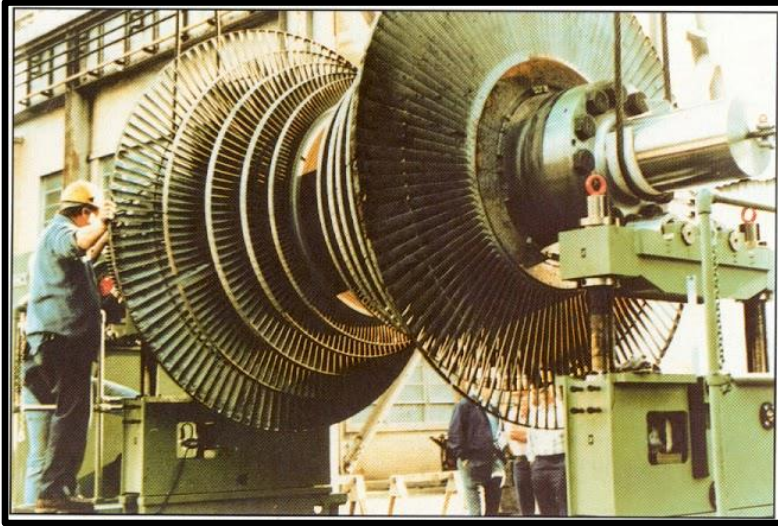


Compressor load torque characteristics

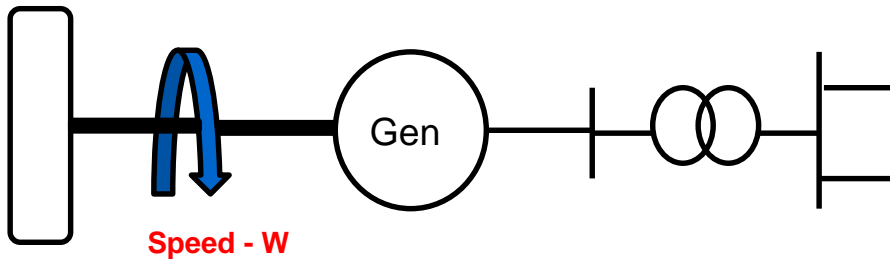


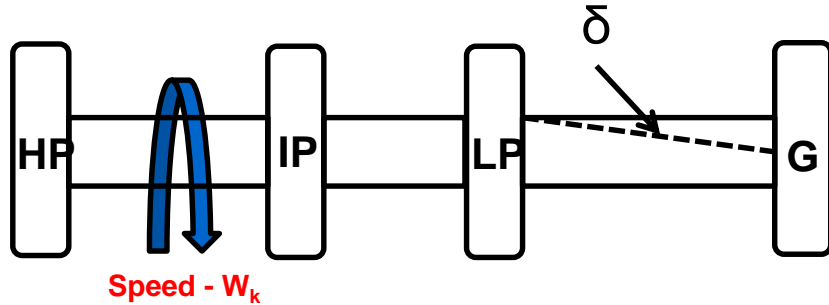
Voltage flicker measured at transmission level



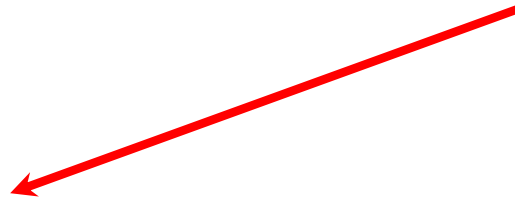
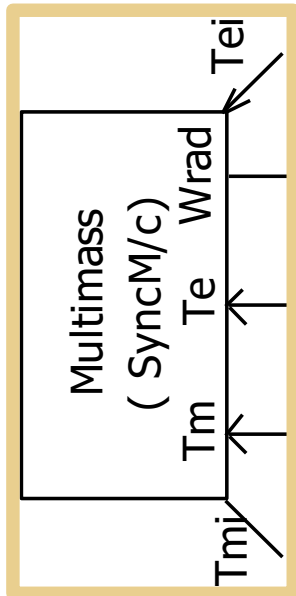


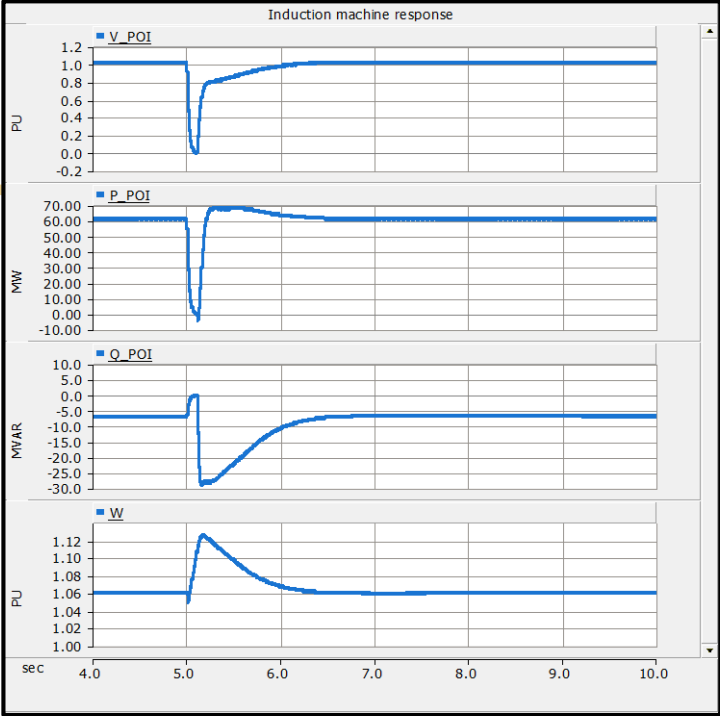
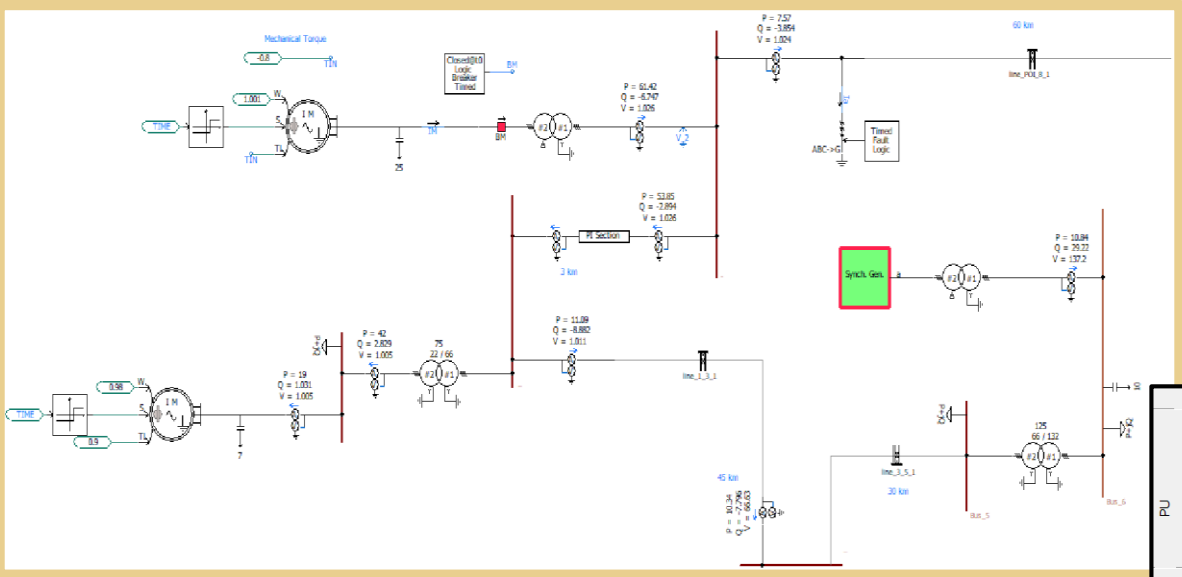
- Rotor of a Turbine Generator is a complex system of masses connected by shaft sections
- The total length can be as much as 50 m.
- A single lumped inertia representation is typically considered in system transient stability studies
  - Assumption: Rigid shafts





- Torsional Interaction studies require a more detailed representation of the shaft (compared to lumped mass representation)
  - A **Multi-Mass** representation
    - Main rotor components represented as separate (rigid) masses
    - The masses are connected to each other with 'elastic' shaft sections







Thank you